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### NOISE COMPARISON OF TWO 1.2-PRESSURE-RATIO FANS WITH 15 AND 42 ROTOR BLADES

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### SUMMARY

In this report, two 1.829-meter- (6-ft-) diameter fans suitable for a quiet engine for future short-takeoff-and-landing (STOL) aircraft were compared. Both fans were designed for a 1.2 pressure ratio with similar weight flows, thrusts, and tip speeds. The first fan, designated QF-9, had 15 rotor blades and 11 stator blades. The rotor was highly loaded and the tip solidity was less than 1. The QF-9 rotor blades had an adjustable-pitch feature which can be used for thrust reversal. The second fan, designated QF-6, operated at a moderate loading with a rotor tip solidity greater than 1. Fan QF-6 had 42 rotor blades and 50 stator blades. The low number of rotor blades for QF-9 reduced the frequency of the blade-passage tone below the range of maximum annoyance. In addition to this difference, the QF-9 fan had a somewhat smaller rotor-stator separation than the QF-6 fan.

In terms of sound pressure level and sound power level, QF-9 was the noisier fan, with the power level results for QF-9 being about 1 decibel above those for QF-6 at equivalent operating points as determined by similar stage pressure ratios. At these same equivalent operating points, the maximum perceived noise along a 152.5-meter (500-ft) sideline for QF-9 was about 2.5 PNdB below that for QF-6, which indicated that QF-9 was less objectionable to human hearing.

### **INTRODUCTION**

Short-takeoff-and-landing (STOL) aircraft of the future are planned for operation near highly populated areas. The reduction of engine noise is therefore a very important consideration that will largely dictate the engine design. In this report, two candidate 1.829-meter- (6-ft-) diameter, low-tip-speed fans for a low-noise engine are compared. One fan, designated QF-9, features an unusually low number of rotor and

stator blades with high rotor blade loading. In addition, the QF-9 rotor blades have an adjustable-pitch feature which provides an unconventional method of thrust reversal for fans. The second fan in this comparison, designated QF-6, is a fixed-pitch fan that has a higher number of blades with moderate loading.

The low number of rotor blades on QF-9 was expected to yield a noise benefit in reducing the frequency of the blade-passage tone relative to that of QF-6, since the shaft rotation speeds were about the same. If it is assumed that the level of the tone is unchanged, the tone at low frequency is less annoying than a high-frequency tone. This result would be reflected in a lower calculated perceived noise level. This study compares the two fans in terms of sound pressure level, directionality, and perceived noise.

### **APPARATUS**

### Fan Assemblies

The acoustic and aerodynamic data in this report are for the design nozzle configurations. Fan QF-6 was designed by NASA; fan QF-9 was a contractor design. The specific design approaches differed for the two fans. In table I, selected design configuration parameters are compared for the two fans. In addition to a 1.2 pressure ratio, both fans were designed for approximately the same weight flow, thrust, and tip speed. Fan QF-9 is much more highly loaded than QF-6 as shown by the D-factor, which has a maximum of 0.530 for the QF-9 rotor compared to a maximum of 0.386 for the QF-6 rotor. The D-factor remains at a high level over the entire length of the QF-9 rotor. The QF-9 rotor and stator chords are considerably longer than those of QF-6. Fan QF-9 was designed by Hamilton-Standard.

Figures 1 and 2 show the blading of the conventional fan, QF-6. In figure 1, the view of the partially assembled stage shows the 42 fixed-pitch blades of the rotor. Figure 2 shows part of the 50-blade stator assembly.

Figure 3 and 4 show the blading of QF-9. Figure 3 shows part of the 15-blade rotor assembly. The chord of these blades increases from hub to tip, with a maximum value of 34.3 centimeters (13.5 in.) at the tip. These blades have an adjustable-pitch feature, although for this comparison the rotor blades remained at the design setting. The partially assembled QF-9 stator, shown in figure 4, clearly shows the very-low-solidity, large-chord blading. The adjustable-pitch feature of QF-9 was not feasible for QF-6 because of mechanical complexities required to actuate such a large number of blades.

Figure 5 presents the relative positions of the QF-6 and QF-9 blading as viewed looking toward the fan axis from the blade tips. To reduce rotor-stator wake inter-

action, a major noise-generating mechanism, it is desirable to increase the axial spacing between these blade rows. For QF-6, the spacing is about four rotor-chord lengths. However, the large-chord blades limited the practical spacing for QF-9 in the facility to about two rotor-chord lengths at the tip. The large camber of the QF-9 blades resulted primarily from the lower solidity levels for that design (table I(b)). Differences in blade camber and chord angle are more pronounced for the stator blade because of large differences in design incidence angle for the two designs.

Figure 6 is a cutaway sketch of a typical fan installation as tested at the NASA Quiet Fan Facility. The sketch is a schematic representation showing the drive shaft in the fan inlet and the support pylon. In all testing, the fan flow passage was completely hard, that is, with no acoustic suppression treatment.

### Facility

The fans compared in this report were tested at the NASA Quiet Fan Facility, shown in figure 7. The fans are located on a concrete pedestal 37 meters (121 ft) from the face of the wind tunnel drive motor building. The wind tunnel drive motors are used to drive the fan through a gearbox and drive shaft. The acoustic data were taken with an array of microphones located at the fan centerline elevation on a 30.5-meter (100-ft) radius from the fan at 10° increments from 10° to 160° from the fan inlet centerline. Data were not taken at 0° because of the presence of the drive shaft, nor above 160° because of high-velocity fan exhaust. In figure 7, the microphones are shown covered with plastic bags as weather protection. Foam treatment is shown on the portion of the drive motor building wall that was considered likely to cause a sound reflection problem at the microphone locations. Figure 8 is a sketch of the test site. The entire test site surface was hard asphalt.

### Instrumentation

Both fans had several similar measuring stations to allow a measurement of the fan aerodynamic performance. Figures 9 and 10 show the axial locations of the measurement stations on QF-6 and QF-9, respectively. Figure 11 shows the detailed layout of this instrumentation at each of the four measuring stations. Six equally spaced thermocouples were located on the lip of the bell-mouthed inlet to determine the average inlet temperature. Six static taps were located in the outer wall of the inlet duct. These static taps were used for the inlet weight flow calculation. Four identical total pressure and temperature rakes were used downstream of the stator blade row to determine the stage weight flow and the stage total pressure ratio. These rakes were located nominally

at 90° intervals but were displaced slightly in order to avoid being in a stator wake. Finally, just downstream of the nozzle exit, three equally spaced total pressure rakes were used for thrust measurements. These three rakes were arranged as shown to avoid the wake from the support pylon. All rakes were removed for acoustic tests.

### PROCEDURE AND DATA REDUCTION

The aerodynamic data were recorded through a pressure multiplexing valve, a pressure transducer, and a computer network. This system recorded nine samples in about 90 seconds. These raw data samples were averaged and used to compute the desired flow parameters.

Three separate 100-second samples for each speed point were recorded from the microphone data on magnetic tape for later analysis. Simultaneously with the magnetic tape recording, an on-line one-third-octave-band analyzer was used for 4 seconds on each microphone sample, and the results were recorded on digital tape. These one-third-octave digital data were further adjusted for atmospheric absorption to obtain results corrected to standard-day conditions of 15°C and 70 percent relative humidity. The data were not adjusted for ground reflection. From these standard-day, sound pressure level data, the sound power level and perceived noise values were calculated. For the perceived noise level determinations, the data were adjusted to a 152.5-meter (500-ft) sideline, which has become standard practice for STOL noise evaluations. A more detailed discussion of the acoustic data analysis for the Quiet Fan tests is given in reference 1.

### RESULTS AND DISCUSSION

### Aerodynamic Performance

At a given percent of design speed, the total pressure ratio of the QF-6 fan was slightly higher than that of the QF-9 fan. The design inlet weight flow of 396 kilograms per second (873 lbm/sec) was achieved with QF-6, but a stage pressure ratio of only 1.182 was obtained rather than the design-predicted 1.2. The measured thrust of QF-6 was 59 575 newtons (13 393 lbf), which is below the design value of 70 415 newtons (15 830 lbf). As shown in table II, the performance of QF-9 also fell somewhat short of the design-predicted values of weight flow and pressure ratio. The measured weight flow was 388 kilograms per second (855 lbm/sec), as compared to the predicted 403 kilograms per second (889 lbm/sec); the measured thrust was 56 412 newtons (12 682 lbf), as compared to the predicted 71 705 newtons (16 120 lbf); and the pressure

ratio at design speed was 1.170. Throughout this report, the fan-stage total pressure ratio is used, as well as the percent of design speed, as a means of correlating the acoustic data of the two fans. To achieve a higher pressure ratio, QF-9 was run at speeds above its design speed.

### Perceived Noise Directionality

Figure 12 is a series of five plots which compare overall perceived noise level (PNL) as a function of angle on a 152.5-meter (500-ft) sideline for the two fans at various speeds. In each plot, the two-lobe nature of the noise is evident, with both fans being rear-quadrant dominated. Figure 12(a) compares the two fans at 60 percent of their design speeds. At all angles except 10° along the sideline, QF-6 has the higher perceived noise level, with the difference being especially marked in the rear quadrant. At 60 percent of design speed, the pressure ratio of QF-6 is slightly above that of QF-9.

At 70 percent of design speed, figure 12(b), both fans produce about the same PNL's in the front quadrant, with QF-6 again dominating the rear quadrant. Again, QF-6 has the slightly higher stage pressure ratio.

QF-9 was run at 86 and 93 percent of design speed rather than at the 80- and 90-percent speed points of QF-6, which had been run earlier. Eighty-six percent of design speed was specified by the fan-stage designer as the approach speed, with 93 percent of design speed being selected as an additional point between the approach and 100-percent (takeoff) speed. In figure 12(c), the results for QF-6 at 80 percent of design speed are compared with those for QF-9 at the existing 70- and 86-percent speeds. In the front quadrant, QF-6 at 80-percent speed has only a slightly higher PNL than QF-9 at 70-percent speed. In the rear quadrant, the results of QF-6 compare very closely with the results of QF-9 at 86-percent speed; although the QF-9 pressure ratio is higher, 1.125 compared to 1.080 for QF-6.

At 90 percent of design speed, figure 12(d), the QF-6 results compare closely in PLN level with the results of QF-9 at the existing 86- and 93-percent speed at the front angles. In the rear quadrant, the noise of QF-6 dominates both QF-9 cases.

Finally, in figure 12(e), the results of QF-6 at 100 percent of design speed are compared with the results of QF-9 at both design speed and 110 percent of design speed, where the QF-9 pressure ratio is 1.210 - slightly above its predicted design value. At 100-percent speed, QF-6 is still the noisier fan at all angles.

### Sound Pressure Spectra

The low number of rotor blades in the QF-9 design was expected to lower the QF-9

blade-passage-tone frequency (BPF) to a region of less sensitive human hearing. The sound pressure level spectra show the frequencies of the fan's blade-passage tones. The one-third-octave sound pressure level (SPL) spectra corresponding to the peak angular overall sound pressure levels (OASPL) are compared in figure 13 for the front quadrant and in figure 14 for the rear quadrant. Comparisons are made in the same manner with respect to speeds as were the PNL distributions of figure 12. In figures 13 and 14, however, the data are for the 30.5-meter (100-ft) microphone radius rather than a 152.5-meter (500-ft) sideline.

Front quadrant. - The blade-passage-tone spikes (BPF) and the first overtone, or second harmonic (2H), are designated for each spectrum. In some cases, a shift in fan speed is not enough to place the blade-passage tone in a different one-third-octave filter. Hence, the tone SPL appears to be at the same frequency for two speeds. Figure 13 presents the SPL spectra at the angle of maximum OASPL in the front quadrant; figure 14 presents the SPL spectra at the angle of maximum OASPL in the rear quadrant. In each comparison, the blade-passage tone for QF-9 is clearly at a much lower frequency than for QF-6 because of the fewer number of rotor blades.

The front-quadrant spectra at 60 and 70 percent of design speed are shown in figures 13(a) and (b); the QF-9 SPL is above the QF-6 SPL from 200 hertz to about 1000 hertz and below the QF-6 SPL at higher frequencies. Also, the level of the blade-passage-tone spike is higher for QF-9 than for QF-6 at these two speeds.

Figure 13(c) compares the SPL spectrum for QF-6 at 80 percent of design speed with the spectra for QF-9 at 70 and 86 percent of design speed. It is noteworthy that the blade-passage-tone spike is at a much higher SPL for both QF-9 cases than for QF-6, even though the QF-9 pressure ratio at 70-percent speed is only 1.081, compared to the QF-6 80-percent-speed value of 1.117. QF-6 has a higher SPL at all frequencies above 1200 hertz.

Figure 13(d), comparing the results of QF-6 at 90-percent speed with the results of QF-9 at 86 and 93 percent of design speed, shows the same high relative levels for the QF-9 blade-passage tones. Otherwise, in figure 13(d), QF-9 is seen to be the dominant noise source to about 1600 hertz, with QF-6 being the noisier fan above this frequency.

Finally, figure 13(e) compares the SPL spectrum for QF-6 at design speed with the design-speed and 110-percent-speed spectra of QF-9. The QF-9 levels continue to dominate to about 1600 hertz. Above 1600 hertz, the noise of QF-6 has the higher SPL. There is little difference between the two QF-9 spectra at frequencies above 1600 hertz.

In general, the QF-9 sound pressure levels are higher than the QF-6 levels at low frequencies, to about 1000 hertz, with QF-6 having the higher levels at the higher frequencies. These differences in SPL are caused by the relative locations of the blade-passage tones for the two fans. In addition, the internal broadband noise which is relatable to the blade chord lengths (ref. 2) is expected to be lower in frequency for QF-9 than for QF-6 because of the larger rotor-chord lengths of QF-9.

Rear quadrant. - Figure 14 presents the same type of comparison for the rear quadrant that figure 13 presents for the front quadrant. In the front quadrant, figure 13, QF-9 typically has a higher blade-passage SPL level than QF-6. In the rear quadrant, the blade-passage spikes are at nearly the same levels.

Beginning with the 60-percent-speed comparison of figure 14(a), the QF-9 results as usual dominate to about 1000 hertz; the results of QF-6 dominate above this frequency. The blade-passage-tone SPL for QF-6 is slightly higher than that for QF-9.

At 70-percent speed, figure 14(b), the blade-passage tone SPL's have nearly the same level for QF-6 and QF-9.

Figure 14(c) compares the results of QF-6 at 80-percent speed with the results of QF-9 at 70- and 86-percent speed. Here the level of the blade-passage tone of QF-6 falls between the levels for the QF-9 blade-passage tones at 70- and 86-percent speed. The QF-6 SPL is above both QF-9 cases at frequencies above 1600 hertz, although there is a marked increase in the higher frequency SPL of QF-9 as its speed is increased from 70 to 86 percent.

In figure 14(d), comparing data for QF-6 at 90-percent speed with the data for QF-9 at 86- and 93-percent speed shows that the blade-passage-tone SPL's are nearly the same.

Finally, in figure 14(e), comparing the SPL for QF-6 at design speed with the SPL for QF-9 at design and 110-percent speed shows that the QF-9 SPL is much greater than the QF-6 SPL at the lower frequencies (<1600 Hz). Only in the 110-percent-speed case does the QF-9 blade-passage-tone SPL slightly exceed the blade-passage-tone SPL for QF-6. In this case, QF-9 has a pressure ratio of 1.210 compared to 1.182 for QF-6. At the higher frequencies, QF-9 at 110-percent speed nearly matches the SPL of QF-6.

Thus, the maximum rear-quadrant noise data of figure 14 show that the BPF tones for the two fans are about equal and that the broadband noise of QF-9 is greater than that of QF-6 at all frequencies to the QF-6 BPF. At all higher frequencies, the QF-6 broadband is higher except for at 110-percent speed, where the level of QF-9 is about equal to that of QF-6 at 100-percent speed.

### Narrow-Band Spectra

The front- and rear-quadrant tape-recorded data were also analyzed with a constant 32-hertz-bandwidth narrow-band analyzer and are presented in figure 15. These detailed spectra show the blade-passage tones (designated BPF) and the associated harmonics much more clearly than did the one-third-octave analysis. The data presented in figure 15 were not corrected for standard-day conditions. The measurements were taken at a 30.5-meter (100-ft) radius from the fan. In figure 15(a), the results of QF-6 and QF-9 at design speed are compared at 20°, as a typical angle. As in the one-third-

octave front-quadrant spectra of figure 13, the blade-passage-tone SPL of QF-9 is above that of QF-6. At frequencies above the QF-6 BPF, the broadband noise of QF-6 has the higher level, reaching an almost constant 4 decibels higher than the QF-9 SPL above 4000 hertz. Figure 15(b) compares the results of QF-6 at design speed and QF-9 at 110-percent speed at 20°. At this front-quadrant position, the QF-9 SPL's at 110-percent speed are very nearly the same as the QF-9 SPL's observed at design speed (fig. 15(a)), except for the blade-passage-tone level, which is slightly higher at the 110-percent speed. These same comparisons are made at a typical rear-quadrant angle, 130° in figures 15(c) and (d). Figure 15(c) compares the design-speed spectra for the two fans. At this rear-quadrant position, the QF-6 SPL assumes an almost constant 7-decibel increase over the corresponding QF-9 design-speed SPL above 4000 hertz. Finally, in figure 15(d), the QF-9 110-percent-speed SPL results are at about the same levels as the QF-6 design-speed results at frequencies above 4000 hertz. Note that in the rear quadrant (at 130°) the QF-9 110-percent-speed SPL levels are above the QF-9 design-sped SPL's, while in the front quadrant (at 20°) increasing the QF-9 speed from design to 110 percent had little effect on the sound pressure levels.

### Power Level Spectra

The sound power level (PWL) spectra, integrated from 10° to 160°, are presented in figure 16. The comparison at 60-percent speed, figure 16(a), shows the bladepassage tones for both fans at the same power level. Otherwise, as noted for the SPL's, QF-9 has the higher sound power level below 1000 hertz and QF-6 has the higher level at the higher frequencies. At 70 percent of design speed, figure 16(b), the QF-9 bladepassage tone is now above the level of the QF-6 tone. In figure 16(c) with QF-6 at 80-percent speed and QF-9 at 70- and 86-percent speed, the results of QF-6 still dominate above 2000 hertz. The QF-9, 70-percent-speed-spectrum, blade-passage-tone PWL is about the same as that for QF-6; the tone PWL for the 86-percent-speed spectrum is considerably above the QF-6 level. Figure 16(d) compares the 90-percentspeed spectrum of QF-6 with the 86- and 93-percent-speed spectra of QF-9; again QF-9 clearly dominates the lower frequencies, and QF-6 the higher frequencies. The QF-9 blade-passage-tone PWL at both speeds is above the QF-6 level. Finally, at the design speed for QF-6 and both design speed and 110-percent speed for QF-9, figure 16(e), the QF-9 results still dominate the low-frequency PWL spectra. At higher frequencies, QF-6 is still the noisier fan, but the difference between QF-6 and QF-9 is less than at the lower speeds. At design speeds, the QF-6 blade-passage-tone PWL is slightly greater than the QF-9 value. However, the blade-passage-tone PWL of QF-9 at 110-percent speed is well above that of QF-6 at design speed.

The appendix introduces computer tabulation and plots of the acoustic data. These tables and plots can be found at the end of this report.

### Overall Correlations

Throughout this report, the percent of design speed and the stage pressure ratio have been used to identify the sound data test points. Figure 17 relates the overall sound power level (OAPWL) to the percent of design speed for both fans. In this comparison, both fans seem to have about the same OAPWL at any given speed from 60 percent to design speed. The slope of the QF-9 OAPWL curve has an inflection before the increase to the overspeed points.

Perhaps a more meaningful way to correlate these data, considering the actual stage performance, is to plot the OAPWL against the stage pressure ratio. This is done in figure 18. Now QF-9 is seen to produce a slightly higher OAPWL (about 1 dB higher) for a given pressure ratio to the design-speed point of 1.170 pressure ratio. This higher OAPWL might have been caused by the higher loading levels and closer rotor-stator spacing of QF-9 compared to QF-6. Again, the overspeed data show a continued increase in OAPWL.

The maximum perceived noise levels along a 152.5-meter (500-ft) sideline are plotted as a function of the percent of fan design speed in figure 19 and as a function of the stage pressure ratio in figure 20. In figure 19, the maximum sideline PNL is about 2.5 PNdB lower for QF-9 than for QF-6 at similar fan speeds. When this maximum sideline PNL is plotted as a function of the stage pressure ratio, as in figure 20, QF-6 still has the higher noise level. However, the PNdB difference between the two fans is not as great as in the comparison of figure 19. Thus, the use of the small number of blades in QF-9 did achieve a small measure of perceived noise relief by shifting the noise to a lower frequency range, a region of lower human ear sensitivity.

### CONCLUDING REMARKS

Two candidate fans (QF-9 and QF-6) for a quiet, short-takeoff-and-landing (STOL) aircraft were compared for acoustic performance. Fan QF-9 is a highly loaded design, with a solidity less than 1, that uses a low number of rotor and stator blades. The very low number of rotor blades (15) lowers the blade-passage frequency and allows QF-9 to have an adjustable-rotor-pitch feature which can be used for thrust reversal. The second fan in the comparison, QF-6, has a high solidity and moderate loading with a higher number of rotor (42) and stator blades. Both fans were designed for a 1.2 stage pressure ratio and similar tip speeds and weight flows.

Neither fan achieved the design stage pressure ratio; QF-6 came closer, with a pressure ratio of 1.182 compared to 1.170 for QF-9. Fan QF-6 achieved its design inlet weight flow at design speed, but QF-9's measured weight flow at design speed was slightly below the predicted value.

The sound pressure level and sound power level spectra for QF-6 and QF-9 at similar stage pressure ratios and fan speeds show QF-9 to be consistently noisier at the lower frequencies ( $\lesssim 1000 \text{ Hz}$ ), depending on the fan speed. Fan QF-6 is noisier at the higher frequencies.

In the front quadrant, the blade-passage-frequency sound pressure level was consistently higher for QF-9 than for QF-6; in the rear quadrant, the tones were very nearly at the same level for the two fans. Both fans had higher perceived noise levels in the rear quadrant than in the front quadrant at all speeds. As a function of percent of fan design speed, both fans produced about equal overall sound power levels. However, because of the somewhat lower pressure ratios of QF-9 as a function of speed, QF-9 has a somewhat higher overall sound pressure level than QF-6 at a given pressure ratio.

The main acoustic result of the reduced number of blades on QF-9 was to lower its major noise contribution, the blade-passage tone, to lower frequencies where it is less objectionable to human hearing. In terms of preceived noise levels, QF-9 was less objectionable than QF-6, especially in the rear quadrant.

The low-blade-number approach used in the QF-9 design shows promise as a method of reducing the perceived noise level of a quiet STOL engine. Also, the variable-pitch feature, made practical by the low number of blades in QF-9, could be a considerable asset in a future quiet STOL engine.

Lewis Research Center,
National Aeronautics and Space Administration,
Cleveland, Ohio, June 25, 1973,
501-24.

### APPENDIX - COMPUTER TABULATION AND PLOTS OF ACQUISTIC DATA

This appendix introduces computer listings and plots of the acoustic data for QF-6 and QF-9. Figure 21 presents the sound power level (PWL) spectra for QF-6 and QF-9. Figure 21(a) presents the PWL spectra for QF-6 at 60, 70, 80, 90, and 100 percent of design speed. Figure 21(b) presents the PWL spectra for QF-9 at 60, 70, 86, and 93 percent of design speed. Figure 21(c) presents the PWL spectra for QF-9 at 100, 110, 115, and 120 percent of design speed.

Figures 22(a), (b), and (c) present the corresponding overall sound pressure level distribution on a 30.5-meter (100-ft) radius for QF-6 and QF-9.

Figures 23(a), (b), and (c) present the corresponding perceived noise on a 30.5-meter radius for QF-6 and QF-9.

Figures 24, 25, and 26 present the one-third-octave sound pressure level spectra at each angle from  $10^{0}$  to  $160^{0}$  from the fan inlet.

Table III is a listing of the acoustic data for QF-6.

Table IV is a listing of the acoustic data for QF-9.

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### TABLE I. - FAN DESIGN CHARACTERISTICS

### (a) Aerodynamic design parameters

Parameter	QF-6	QF-9
Overall total pressure ratio	1.20	1.20
Rotor-stator separation, number of rotor chords	4.0	~2.0
Predicted overall efficiency, percent	87.9	90.2
Corrected inlet weight flow, kg/sec (lbm/sec)	396 (873)	403 (889)
Corrected inlet specific weight flow, kg/(sec)(m <sup>2</sup> ) (lbm/(sec)(ft <sup>2</sup> ))	181.6 (37.4)	194.8 (39.9)
Thrust, N (lbf)	70 415 (15 830)	71 705 (16 120)
Work coefficient	0.338	0.369
Rotor head-rise coefficient	0.311	0.348
Stage head-rise coefficient	0.298	0.334
Corrected rotor tip speed, m/sec (ft/sec)	229 (750)	213 (700)
Tip diameter, m (ft)	1.829 (6.0)	1.829 (6.0)

### (b) Blade design parameters

Parameter	QF	-6	QF	-9
	Rotor	Stator	Rotor	Stator
Number of blades	42	50	15	11
Chord, cm (in.):				
Hub	17.5 (6.89)	11.7 (4.61)	21.5 (8.46)	38.1 (15.0)
Tip	16.3 (6.40)	11.7 (4.61)	34.3 (13.5)	38.1 (15.0)
Solidity:			,	
Hub	2.827	1.752	1.219	1.406
Tip	1.188	1.000	0.893	0.714
D-factor:	}			·
Hub	0.151	0.417	0.530	0.512
Maximum	0.386	0.417	0.530	0.512
Tip	0.357	0.301	0.431	0.363
Cruise design corrected speed, rpm	2387.2		2227.0	
Rotor blade-passage frequency, Hz	1671		557	
Camber angle, deg:				
Hub	36.15	34.11	44.89	52.50
Tip	8.98	15.83	18.40	56.40
Chord angle relative to fan axis, deg:				
Hub	6.12	10.77	5.61	16.30
Tip	43.04	2.07	41.14	11.92
Aspect ratio, mean	3.08	3.46	1.70	1.23
Rotor inlet hub-tip radius ratio	0.416		0.460	
Tip relative inlet Mach number	0.878		0.865	
Mater al	Aluminum	Aluminum	Plastic/	Aluminum
		L	titanium	

TABLE II. - SELECTED AERODYNAMIC PARAMETERS AT DESIGN SPEED DESIGN PREDICTION COMPARED WITH MEASURED RESULT

Parameter	QF-6	QF-9
Design corrected tip speed, m/sec (ft/sec)	229 (750)	213 (700)
Corrected inlet weight flow, kg/sec (lbm/sec):		
Design	396 (873)	403 (889)
Measured	397 (875)	388 (855)
Total pressure ratio:		
Design	1.2	1.2
Measured	1.182	1.171
Thrust, N (lbf):		
Design	70 415 (15 830)	71 705 (16 120)
Measured	59 575 (13 393)	56 412 (12 682)

## TABLE III. - FAR-FIELD NOISE OF QF-6 WITH DESIGN NOZZLE

[Data adjusted to standard day of  $15^{\rm o}$  C and 70 percent relative humidity; SPL re  $2\times10^{-5}\,{\rm N/m}^2$ ; PWL re  $10^{-13}\,{\rm W.}$ ]

(a) Percent of design speed, 60; fan physical speed, 1445 rpm; fundamental blade-passage frequency, 1011 hertz.

FRECKENCY								ANGL	E, DEG								AVERAGE	3
	10	20	30	07	20	09	02	80	06	100	110	120	130	140	150	160		(PWL)
			1,	/3-0CT	AVE BA!	ND SCUP	UND PRE	SSURE	LEVEL	(ISPL)	ON 30.	5-METE	R RADIO	US				
20 E	72.5 67.2 7C.5	89.5 67.5 81.0	65.0 66.0 68.8	69.4 65.2 66.3	70.5 66.5 65.8	70.5 67.7 66.8	70.5 66.3 66.5	67.4 65.7 65.8	69.7 65.7 65.8	69.0 64.5 65.6	70.4 65.7 66.1	67.8 66.4 68.1	68.8 66.3 67.8	70.7 68.0 69.1	69.9 68.0 69.8	69.2 68.2 70.2	69.8 66.8 68.0	116.8
100	76.5 71.8	73.6 73.6	67.3 72.1 71.8	67.1 71.5 70.5	65.6 70.0 68.5	66.6 70.6 69.2	66.3 68.6 68.3	66.0 68.1 67.8	66.0 68.5 68.0	66.0 69.6 68.8	67.1 70.6 69.7	67.9 69.9 70.8	67.5 70.8 69.0	69.3 71.0 69.7	69.6 69.5 68.7	69.7 69.2 68.1	69.7 75.0 70.5	114.6
20C 25C 33.5	72.2	72.4 75.0 75.1	65.9 72.7 72.2	68.2 71.2 70.7	67.2 67.7 68.9	66.4 67.7 68.9	65.9 66.0 67.6	66.0 66.4 68.4	65.9 67.7 68.2	65.5 68.4 69.7	66.2 69.9 70.7	67.5 72.0 71.8	67.3 71.8 71.9	68.4 71.2 70.9	67.5 69.0 69.7	67.3 67.3 67.6	68.9 73.7 71.7	114.7 117.2 117.7
4 & & & & & & & & & & & & & & & & & & &	76.5	76.5 78.3 79.5	75.0 77.2 77.8	73.0 75.5 76.6	70.6 73.2 74.6	69.6 71.3 72.1	68.1 70.0 70.6	68.0 70.0 70.8	69.1 70.3 72.1	71.5 73.0 74.0	73:1 74.5 75.6	74.7 75.6 77.0	75.0 76.0 77.8	73•1 74•7 76•5	70.5 71.7 73.6	67.0 68.0 69.8	73.5	119.6 121.2 122.5
80C 10Ce 1250	75.0 85.4 82.7	80.8 91.0 84.5	80.2 89.5 83.0	78.8 88.7 81.4	76.5 87.0 79.4	74.5 84.2 77.0	72.5 83.7 75.0	73.2 82.0 74.9	75.0 85.5 77.4	76.7 87.2 78.7	77.8 88.2 80.4	79.6 90.5 82.3	81.3 91.4 83.3	79.0 87.9 81.7	74.7 83.0 77.5	71.9 85.9 74.9	78.0 87.9 80.4	124.9
1800 2000 2500	8 8 8 6 6 6 6 6 6 6 6 6 6 6 6 6 6 7 6 7	88.3 85.8	84.0 87.2 83.8	82.0 85.8 82.6	80.0 84.5 80.6	77.2 81.3 77.6	74.7 77.8 74.6	75.5 77.3 74.8	78.4 80.8 78.0	80.2 83.2 80.0	82.2 85.3 83.0	83.1 86.1 83.9	84.6 87.8 85.5	83.4 87.2 85.0	78.2 82.8 80.6	73.9 78.4 75.5	81.4 84.9 82.3	128.6 132.1 129.6
4 4 10 00 00 00 00 00 00 00 00 00 00 00 00	84.5 84.2 82.1	85.9 85.0 82.4	85.1 84.3 81.2	83.9 83.5 81.2	82.1 81.8 78.9	79.2 78.1 75.9	75.4 74.2 71.6	74.7 74.2 71.2	78.6 77.7 74.9	80.4 79.7 77.4	82.6 82.5 80.7	84.5 83.0 81.5	86.2 84.7 82.3	86.1 84.3 81.4	82.2 80.3 79.7	76.3 74.8 73.2	83.2 4.28 4.4.	130.4
63CC 8OCC 10OCC	86.4 86.4 75.0	81.8 81.1 78.9	86.9 86.1 77.9	79.4 79.6 76.5	77.7 76.6 73.9	75.6 75.1 72.2	70.4 69.1 66.4	69.2 67.6 64.5	74.1 72.9 69.5	75.2 74.6 71.0	78.5 77.4 74.4	79.3 78.1 74.7	80.1 79.9 76.5	. 80•3 79•8 75•8	77.3 76.4 73.2	71.2 70.4 67.0	79.3 77.2	126.5 126.4 124.2
126CC 16CC 200CC	76.6 72.4 65.5	77.1 74.2 69.8	75.6 72.4 68.5	75.1 71.7 67.5	72.3 68.5 64.1	70.1 66.3 61.2	64.5 59.8 55.5	61.9 57.4 53.2	66.6 62.9 57.4	69.1 65.0 61.2	72.6 68.1 63.1	73.8 70.2 64.5	74.8 70.1 66.3	74.0 70.4 66.3	71.1 67.1 62.6	64.8 61.3 57.1	76.9 75.0 73.3	123.9 122.0 120.3
TVERALL	55.4	96.7	95.5	94.4	92.5	89.9	1.18	86.9	90.0	91.8	93.7	95.1	96.4	95.0	91.1	88.9	93.8	140.9
DISTANCE				İ		810	EL INE	PERCE	VED N	1SE	VELS	'	.   ,	,		;	<del>- 1 -</del>	
152.5 PETER	5 67	97 6.	.7 83	.5 85	• 3 85	•7 84	•4 82	•3 82	.4 85	6.6 87	.5	9.1 89	63 8 <sub>9</sub>	.2 86	.4 79	.4 71.	6	

(b) Percent of design speed, 70; fan physical speed, 1685 rpm; fundamental blade-passage frequency, 1179 hertz.

POWER LEVEL (PWL)		117.4 116.6 116.5	117.6 119.9 119.7	117.3 119.3 120.0	121.7 123.5 125.2	126.8 131.3 139.3	131.5 133.6 135.8	133.7 133.7 132.2	131.3 131.2 129.3	129.0 127.1 125.4	144.9	
AVERAGE SPL	<del>,</del>	70.0 69.2 69.1	72.5	69.9 71.9 72.6	74.3 76.1 77.8	79.4 83.9 91.9	84.1 86.2 88.4	86.3 84.8	83.8 81.9	81.6 79.7 78.0	97.5	<del></del>
160		74.5 73.8 74.0	74.4 73.8 72.0	71.0 70.8 70.9	70.4 71.0 72.3	73.0 77.6 85.7	76.1 78.5 80.5	78.3 78.1 76.5	74.8	69.1 65.0 61.1	9.06	.4. 73.
150		73.3 73.2 74.3	74.3 74.3 72.9	72.1 72.3 72.5	72.2 73.1 75.2	75.8 79.4 87.6	79.8 82.3 85.8	82.8 82.3 81.4	80.4 79.4 76.8	75.1 71.1 67.3	93.8	.3 82
140	Sn	72.1 72.2 73.1	73.6 74.3 73.3	71.9 74.1 73.7	75.5 76.2 78.7	80.3 84.7 93.0	85.2 87.9 90.9	88.3 87.5 85.7	84.4 83.7 79.9	78.3 74.3 70.5	98.6	.5 90
130	R RADI	70.1 69.6 71.1	73.0 73.4 72.9	71.1 73.9 73.8	76.2 77.7 79.7	82.3 87.1 95.8	87.2 89.4 91.8	89.3 88.8 86.7	85.1 84.6 81.4	79.6 75.4 71.3	100.3	.9 93
120	S-METE	71.1 70.5 70.4	72.1 73.7 73.7	70.5 73.9 74.1	76.3 77.8 79.8	81.7 87.2 96.1	86.3 88.2 90.4	88.0 87.1 86.3	83.9 83.0 79.9	78.8 75.6 69.8	8.66	.4 93
110	ON 30.	69.1 68.1 67.6	69.6 73.4 72.4	68.9 72.3 73.2	74.7 76.7 79.1	80.5 84.9 92.5	85.3 87.1 88.9	86.6 86.5 85.1	83.4 82.2 79.3	78.1 73.7 68.7	7.16	/ELS
100	(SPL)	69.6 66.9 67.0	69.1 72.4 71.8	68.1 71.4 72.7	74.2 76.1 78.1	79.3 82.7 89.0	83.3 84.9 86.1	84.4 84.3 82.6	80.9 80.1 76.8	74.9 71.1 66.8	95.2	1SE LEV
E, DEG	LEVEL	68.5 66.7 66.1	68.0 71.3 71.4	68.3 70.1 71.8	72.5 74.1 75.9	77.3 81.1 88.5	81.5 83.1 84.1	82.4 82.3 80.2	79.6 78.4 75.2	72.2 68.9 63.2	7.66	ED NO
ANGL B	SSURE 1	67.3 65.7 65.1	66.3 69.3 70.8	68.3 67.9 70.2	70.9 72.6 73.7	75.6 79.9 88.1	78.8 79.6 81.4	79.3 78.8 76.6	74.6 73.4 70.6	68.2 63.9 59.1	91.7	PERCEIV •7 87•
70	D PRE	68.5 67.4 65.3	66.3 69.8 71.1	67.9 67.4 70.2	70.9 72.7 73.4	74.6 78.7 86.1	78.2 79.4 81.8	79.4 78.8 77.2	75.6 74.7 72.4	70.2 65.2 61.0	91.0	ELINE F
09	ND SCUN	68.3 68.4 67.0	67.3 71.4 70.9	67.6 68.4 70.0	71.0 73.6 73.7	75.5 80.4 88.3	80.2 82.3 85.1	82.6 83.2 81.1	80.2 79.7 77.3	75.1 71.0 66.0	93.8	S 101
20	VE PA	68.3 66.7 65.5	66.0 72.1 71.3	68.1 70.3 71.0	72.7 75.6 76.6	78.0 81.9 89.6	82.3 84.9 87.6	84.8 85.3	82.1 81.2 78.4	77.1 73.0 68.5	95.6	.9 89.
40	/3-CCTA	68.5 67.2 66.0	67.6 71.8 72.3	69.1 71.3 72.5	74.5 77.1 78.6	80.1 84.4 92.0	84.8 86.4 88.8	87.1 87.7 85.9	84.2 84.1 81.4	79.4 76.0 72.7	97.8	83 0
30	7	66.3 65.4 67.3	68.6 72.8 73.8	71.6	77.0 79.1 80.1	82.1 85.2 92.1	87.0 88.8 90.1	88.3 88.3	85.7 84.6 82.3	80.6 76.9 72.8	7.36	.5 87.
50		68.0 66.7 68.8	68.8 74.1 74.6	73.8 75.8 75.8	77.0 79.4 81.2	82.1 86.7 94.3	87.3 89.4 90.9	88.6 88.3 86.1	85.6 85.2 82.8	81.1 78.1 73.3	1.66	4 82
10		76.0 75.7 66.0	73.4	75.6	7.17 76.97 75.97	8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	8 4 5 5 6 5 6 5 6 6 6 6 6 6 6 6 6 6 6 6 6	87.1 87.1	84.1 84.2 81.5	86.3 77.1	36.6	71.
FRECLENCY		7.4. A.A.	100 125 160	25C 315	460 500 630	8CC 10CC 125C	16CC 20CC 25CC	215C 40CG 50CC	63CC 8CCC	125CC 16CCC 2COOC	CVERALL	DISTANCE 152.5 WETERS

TABLE III. - Continued. FAR-FIELD NOISE OF QF-6 WITH DESIGN NOZZLE

[Data adjusted to standard day of  $15^{\rm o}$  C and 70 percent relative humidity; SPL re  $2\times10^{-5}$  N/m<sup>2</sup>; PWL re  $10^{-13}$  W.]

(c) Percent of design speed, 80; fan physical speed, 1926 rpm; fundamental blade-passage frequency, 1348 hertz.

								70.11	70.0								10 A A A A A A A A A A A A A A A A A A A	2 4
	10	50	30	40	20	. 60	70	80	06	100	110	120	1:30	140	150	160		(PWL)
				1/3-0CT	FAVE' BA	ND SCUN	ND PRE	SSURE	LEVEL	(SPL)	ON 30.	S-METE	R RADI	US.		,		
rii ko ii Di ku ii	71.4	68.7 74.7 69.6	69.7 69.2 69.5	69.4 68.4 68.1	70.0 69.4 68.1	69.2 69.5 67.8	70.5 70.4 67.8	71.2 71.5 68.3	71.4 71.4 68.8	71.0	72.5 74.4 71.5	74.3 73.4 73.9	74.0 74.7 75.0	75.9 75.9 76.6	76.9 76.9 78.1	77.9 78.4 79.5	72.7 73.2 72.6	120.1 120.6 120.0
100 125 160	72.8	71.3 77.1 78.1	70.7 76.3 76.2	70.0 75.1	69.3 74.5 75.6	69.5 73.5	69.5 73.5 73.7	69.8 73.1 73.7	71.274.5	72.7 76.0 75.1	74.2 76.1 76.2	75.9 77.2 76.8	77.0 77.1 76.7	78.7 78.6 76.7	78.7 78.5 76.7	79.6 78.4 76.9	74.2 76.0 75.7	121.6 123.4 123.1
256 256 335	76.5	76.2 79.2 78.6	73.5 76.2 76.2	72.4 74.0 76.1	71.9	71.2	71.2 70.7 72.7	71.7771.5	71.7 73.0 74.9	72.0 74.0 76.1	72.7 75.7 76.7	74.1 76.9 77.7	74.9 77.5 77.4	76.0 76.9 76.4	76.7 76.2 76.6	76.2 74.9 75.3	73.5 75.1 75.9	120.9 122.5 123.3
400 900 900	8C.C 81.1	79.6 81.4 83.2	79.3 80.3 81.7	77.6 79.3 80.8	75.6 78.1 79.5	74.3 75.6 76.8	76.3	74.5 76.3 77.3	75.1 76.9 79.2	76.8 78.4 80.5	78.1 79.9 82.3	79.2 80.9 83.1	79.3 80.4 82.3	77.8 78.4 80.5	75.8 76.3 78.3	74.2 74.5 75.6	77.2 78.7 80.5	124.6 126.1 127.9
800 1000	0 0 0 11 4 11 0 4 11	84.5 85.6 94.0	84.2 84.3 94.2	82.4 83.3 95.5	80.2 81.4 93.5	78.0 79.6 89.7	77.9 79.1 88.5	79.4 80.4 87.3	80.9 82.1 91.8	82.2 83.8 92.0	83.4 84.6 94.3	84.4 86.5 99.8	84.5 85.9 98.7	81.9 82.9 93.5	78.5 78.9 91.3	76.1 77.6 87.2	82.0 83.4 94.5	129.4 130.8 141.9
1600 2000 2500	85.5 95.5 96.5	90.2 90.7 92.0	90.2	89.8 88.5 91.9	87.5 86.5 90.7	84.8 84.8 87.7	83.3 82.2 85.0	83.2 83.2 85.2	86.7 85.8 87.0	87.7 88.2 89.5	89.3 89.2 91.0	93.1 90.4 94.1	92.8 91.8 95.0	89.0 88.2 92.2	85.2 83.5 87.2	81.6 80.6 83.1	89.0 88.2 91.1	136.4 135.6 138.5
# 400 m # 400 m # 400 m # 400 m	86.1 86.5	90.6 91.6 88.9	90.4 91.1 87.9	90.3 91.9 89.6	88.3 89.9 87.1	86.6 87.7 84.9	83.6 84.1 81.4	83.9 84.2 81.6	86.6 86.7 84.3	88.1 88.6 86.6	89.9 90.2 88.3	91.4 91.0 90.1	92.6 92.2 90.3	89.8 89.2 87.6	84.8 84.7 83.6	81.3 81.0 79.2	89.0 90.0 88.2	136.8 137.4 135.6
63CC 80CC 100CC	87.0	88.5 88.5 65.9	87.8 87.6 85.2	88.0 87.9 85.3	86.0 85.3 82.7	85.0 84.8 82.4	80.8 80.3 77.8	79.8 79.1 76.3	83.5 83.5 80.2	85.1 84.6 81.7	86.8 86.4 83.9	87.7 87.2 84.3	88.8 88.4 85.7	86.8 86.4 83.2	82.1 81.8 79.4	77.9 77.5 74.8	87.4 87.7 86.0	134.8 135.1 133.4
125CC 16CCC 2000C	82.0 75.5 76.1	84.7 81.2 76.7	83.0 79.5	83.1 79.7 76.4	81.0 77.1 72.5	80.5 76.3 71.4	75.4 69.9 65.9	73.7 69.4 64.7	77.6 73.9 68.8	79.8 75.8 71.9	82.5 78.4 73.7	83.2 79.9 74.4	83.8 79.4 75.4	81.2 78.0 74.1	78.0 74.3 70.4	73.2 69.4 65.2	85.6 83.7	133. 131. 129.
CVERALL	166.2	101.3	100.8	101.2	99.2	96.8	94.4	94.2	97.3	98.6	100.4	103.4	103.5	100.0	9.96	93.5	100.5	147.
DISTANCE					6	SID	EL INE	PERCE	IVED NO	ISE L	EVELS	0 0	40	7	70	7 76.		

(d) Percent of design speed, 90; fan physical speed, 2167 rpm; fundamental blade-passage frequency, 1516 hertz.

3	( DMC )		123.4 123.1 124.4	125.5 127.0 126.5	124.6 125.9 126.5	127.2 128.4 130.0	131.9 132.7 135.5	137.4	141.6 139.3 138.8	137.8 138.2 136.3	136.0 134.1 132.5	150.3	
AVERAGE	7		76.0 75.7 77.0	78.1 79.6 79.1	77.2 78.5 79.1	79.8 81.0 82.6	84.5 85.3 88.1	97.0 90.0 90.8	94.2 91.9 91.4	90.4 90.8 88.9	88.6 86.7 85.1	102.9	- 2
	160		81.5 82.7 84.4	.84.0 82.7 81.3	80.2 79.0 78.7	77.8 77.5 78.0	78.7 79.5 81.5	90.2 82.6 82.8	85.5 82.7 82.4	81.1 80.6 77.7	76.1 72.5 68.7	96.4	4 80
	150		81.3 80.9 82.8	83.7 83.3 81.1	80.8 80.6 80.2	79.6 79.3 80.5	80.2 80.6 83.2	91.0 84.5 84.8	88.6 86.0 85.8	84.4 84.3 82.4	80.7 77.3 73.5	98.0	.2 86
	140	us .	78.6 78.8 81.6	82.3 82.3 80.6	80.0 80.1 80.2	80.6 80.6 82.6	83.5 83.3 86.1	95.0 88.2 89.5	93.2 90.0 90.3	90.2 89.8 85.9	84.4 80.9 77.2	101.5	.6 93
	130	R RADI	76.8 77.9 79.5	81.0 82.1 80.1	79.0 80.6 80.3	81.6 82.1 83.6	85.8 86.7 89.9	99•3 93•0 93•6	96.7 93.8 93.3	92.0 92.0 88.8	87.0 82.9 79.4	104.8	8 98
ļ	120	5-METEI	78.0 76.9 77.6	79.9 81.2 80.4	78.1 80.2 80.8	81.7 82.9 84.9	86.9 88.1 91.5	101.6 92.9 93.9	96.3 93.7 93.9	91.1 90.8 87.8	87.1 83.8 78.5	105.5	.5 100
	110	ON 30.	75.4 74.3 75.6	77.5. 79.1 79.3	76.7 79.1 79.5	80.6 82.1 84.0	85.8 86.9 90.2	98.5 91.7 92.3	94.1 92.8 91.6	90.2 90.2 87.6	86.5 82.2 78.2	103.5	vel S • 8 99
	100	(SPL)	74.4 74.1 74.0	76.2 78.6 78.1	75.8 77.4 78.5	79.7 81.5 83.1	85.2 86.4 89.1	96.8 90.5 91.3	93.2 92.1 90.8	89.2 88.8 85.6	84.0 80.1 76.3	102.3	1SE LE
E, DEG	. 06	LEVEL	74.4 72.6 73.0	75.0 76.8 78.1	75.3 75.8 78.5	78.1 80.1 82.0	84.0 84.6 86.9	95.0 88.7 89.1	91.7 90.1 88.4	87.5 87.1 84.4	81.5 78.1 72.7	100.5	VED NO
ANGL	80	SSURE	74.4 72.6 72.5	72.8 76.0 76.8	74.8 74.3 77.7	77.1 79.5 80.6	82.5 83.3 85.1	92.2 86.0 86.8	89.4 87.3 85.6	83.7 83.0 80.1	77.9 73.8 69.0	97.9	PERCE 1
٠	70	ND PRE	73.6 71.9 70.6	72.3 76.1 77.1	74.3 74.1 76.7	76.7 78.1 79.6	81.2 82.5 84.4	93.2 85.2 86.0	89.7 86.5 85.6	84.0 83.5 80.9	78.4 73.3 69.0	98.0	EL INE
	09	AND SCUNI	72.8 72.3 71.6	73.2 77.3 77.1	74.5 75.6 76.5	76.6 78.3 79.6	81.2 81.7 85.1	94.7 86.5 87.3	92.1 89.1 88.3	87.0 87.3 84.8	82.6 78.3 72.9	6.66	S1D
	50	AVE B	72.8 71.9 71.1	72.5 77.3 77.8	74.7 76.3 78.3	77.7 79.1 81.3	82.7 83.3 85.9	95.5 88.2 89.1	94.2 90.5 89.6	87.9 87.8 84.9	83.2 79.0 74.0	101.1	95
	40	/3-0CT	72.1 71.6 70.8	73.3 78.5 79.3	75.2 77.3 77.8	79.6 80.6 82.6	84.8 85.0 87.7	97.2 89.5 90.5	95.1 92.3 91.8	89.5 89.8 86.9	84.4 81.3 77.5	102.7	76 90
	30	-	72.4 72.1 71.8	73.7 79.6 75.6	77.0 80.1 79.8	82.1 83.0 83.6	86.7 86.5 88.7	97.3 90.3 90.8	95.7 92.6 90.8	90.5 89.5 87.1	84.7 81.2 77.3	103.0	16 1.0
	20		70.9 72.8 74.6	74.3 80.5 80.9	80.0 83.1 82.2	82.7 83.8 85.1	87.0 87.5 88.9	97.0 91.7 91.6	95.4 92.3 91.3	90.5 90.1 87.4	85.9 82.6 77.7	103.3	5.2 86
	10		72.5	75.0 76.8 86.6	75.8 81.5 81.7	82.5	80 80 80 81 81 L2 81 87 4	95.2 91.3 90.9	92.6 51.0 90.1	86.3	84.4 86.6 76.7	101.7	RS 75
FRECLENCY			riv <b>a</b> m ∩ u α	10C 125 16C	200 250 315	94 P	800 1000 1250	16CC 20C0 2500	9.19.80 9.00 9.00 9.00 9.00	6300 6000 10000	125CC 160CC 200C	CVERALL	DASTANCE 152.5 METER

TABLE III. - Concluded. FAR-FIELD NOISE OF QF-6 WITH DESIGN NOZZLE

[Data adjusted to standard day of  $15^{\rm o}$  C and 70 percent relative humidity; SPL re  $2 \times 10^{-5}$  N/m $^2$ ; PWL re  $10^{-13}$  W.]

(e) Percent of design speed, 100; fan physical speed, 2408 rpm; fundamental blade-passage frequency, 1685 hertz.

10   20   30   40   50   40   70   80   90   100   110   120   130   140   150   160   160   170   173   1	FRECUENCY								ANGL	E, DEG								AVERAGE	POWER
### Contract   Contrac		10	20		07	50	09	70		90	0	7	~ \	(1)	4	r.	જ !		P. F.
100   11-2   10-1   1				1	/3-0CT	AVE BA	ND SC	D PRE	SSURE	Ē	SPL)	30	-METE	R RADI	ns				
125   62.1   83.1   83.9   85.6   74.8   75.3   75.1   75.6   77.5   81.6   81.1   84.4   84.5   86.6   87.5   88.2   81.6   81.1   81.9   83.1   84.9   86.7   85.1   87.5   84.1   81.5   82.1   81.6   81.1   81.9   82.2   82.6   8	A 76 B		80.00	Sign	\$ m \$		244	044	5.0	55.	8 9 9	8 7 8	9.	1:	2. 3.	5.	5.	9.0	127.0 126.4 127.9
### 100   10   10   10   10   10   10	10C 129 16C		380	2 - 2	w 0 %	400	500	N 80 0		-00	9	23.	4 4 4	4 10 10	96.4	7.5	8 4	2.5	129.2 130.3 129.7
### 400   84-5   85-6   85-6   86-2   80-2   80-2   81-2   84-2	266	(4 4 E)	ัต่นก็ตั	.0.60	8	F 6 6	. 4.6	8 9 8		8 6 0	*°°	000	m	26.4	4 4 4	446	4 60	2:0	128.1 129.1 129.4
Section   Sect	4 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	444	ທີ່ທີ່ຕ້	044	ww.4		9.	60"	2.10	₩. 4	4.4	64.9	449	440	w w 4	322	-00	430	130.1 130.8 132.0
1600 96.6 93.9 93.7 94.6 92.6 91.2 90.2 90.3 91.8 93.8 94.6 97.2 98.1 92.3 88.9 86.6 91.2 2000 96.6 93.8 94.6 97.2 98.1 92.3 88.9 86.6 91.2 2000 96.1 91.3 92.8 93.8 94.6 97.2 98.1 92.3 88.9 86.6 91.2 2000 96.1 91.3 90.8 90.4 86.1 83.8 91.8 92.8 92.8 92.8 92.8 92.8 92.8 92.8 92	200	945	ထိထိတိ	7-6		หูหูง	w 4 w	6 13 9	6.5	9 - 8	68.0	60	80 0	٠ 9 9	φ. φ.	200	5	6 7 8	133.9 134.6 136.0
## 4000   91.0   96.8   97.2   96.7   96.0   94.2   93.2   93.2   94.5   95.3   96.3   96.2   91.2   88.8   85.2   93.2   93.2   93.0   94.4   93.4   94.9   96.7   96.2   91.2   93.3   93.3	200		93.	93.	94. 94.	92. 88.	8.7	80.4		8 -10	8 6 8	94.	05. 97. 95.	05. 98. 95.	60.4	w & 0	36.8	01. 94. 91.	148.4 141.4 139.3
## 600C ## 60.0 90.0 90.2 90.3 88.2 88.6 86.3 86.7 90.9 92.2 93.2 94.2 94.6 91.4 86.7 83.3 92.0 93.0 94.0 94.9 91.1 87.1 83.5 93.0 93.0 93.0 94.0 94.9 91.1 87.1 83.5 93.0 93.0 93.0 94.0 94.9 91.1 87.1 83.5 93.0 93.0 93.0 93.0 93.0 93.0 93.0 93.0	. 2588 8613 .	#: ·	300	75.7	900		400	809	0.08	4 E H	W 4 W	F 0. 4	8 9	6.9	6	6 8 8	r. v. 4	9 6 6	143.6
125GC 82.7 84.5 83.5 83.9 82.9 83.1 80.1 81.0 85.2 87.9 90.0 90.2 90.5 86.4 83.7 79.2 91. 16GGC 75.6 81.0 86.1 80.0 78.1 78.5 74.8 77.1 81.7 83.7 86.1 87.3 86.1 83.7 79.7 75.6 89. 20GCC 74.1 75.5 75.4 75.6 72.9 73.0 71.3 72.8 76.7 80.5 81.8 82.0 82.5 80.0 76.7 71.6 87.  EVERABLE 102.0 104.8 105.0 105.6 103.8 102.5 101.7 101.5 103.3 104.7 105.9 108.5 108.8 103.3 100.8 99.4 105.  DISTANCE STANCE 17.4 80.0 94.0 97.4 97.8 98.1 98.3 100.0 101.3 101.9 103.9 102.8 94.9 89.1 82.9	800	-  - u1	6.60	9	9.6	8 - 4	8 8 4	5.20	9 9 6	000	2.6	m m 0	4 4 0	447	8	5.5	m m 0	3.5	140.0 140.4 138.6
EVERAUL         102.0         104.8         105.6         103.8         102.5         101.7         101.5         103.3         104.7         103.9         108.5         108.8         103.3         100.8         99.4         105.4         105.8           DISTANCE         SIDELINE PERCEIVED NGISE LEVELS         SIDELINE SIDELINE NGISE NGIS	250	1754	4	w 0 w	200			4.0		 G	7°°°°°°°°°°°°°°°°°°°°°°°°°°°°°°°°°°°°°	0 9	7.	6.	9.0	9.	5.0	1.	138.5 136.6 135.0
DISTANCE  DISTANCE  SIDELINE PERCFIVED NGISE LEVELS  ES E WEIFD	VERA	: :	04.	95	95.	93	02.5	101	01.5	03.3	04.7	105.	80	80	03.	8	6	05.	153.1
200 THE LEVEL WITH THE PARTY OF	STANCE S WETE	RS 77	6 89	96 0.	16 0.1	76 9.	2 2	.8	PERCE •1 9	3 10 N	1SE L	VELS	.9 10	.9 102	46 8.	6	.1 82.		

# TABLE IV. - FAR-FIELD NOISE OF QF-9 WITH DESIGN NOZZLE

[Data adjusted to standard day of 15° C and 70 percent relative humidity; SPL re 2x10<sup>-5</sup> N/m<sup>2</sup>; PWL re 10<sup>-13</sup> W.]

(a) Percent of design speed, 60; fan physical speed, 1331 rpm; fundamental blade-passage frequency, 332 hertz.

POWER	PW	1	114.9	116.6 120.1 118.8	117.8 123.3 135.6	128.2 126.2 130.7	128.0 129.1 127.3	126.2 124.8 123.0	122.4 122.1 120.9	121.4	119.9 118.3 117.0	140.2	
AVERAGE			67.5 64.8 66.9	69.2 72.7 71.4	70.4 75.9 88.2	80.8 78.8 83.3	80.6 81.7 79.9	78.8 77.4 75.6	75.0 74.7 73.5	74.0	72.5 70.9 69.6	95.8	
	160		68.4 67.9 68.6	68.7 70.2 69.1	69.3 71.7 85.0	75.7 74.8 79.0	75.2	71.9 70.3 68.6	67.9 67.6 65.1	65.5 65.1 62.4	59.9 57.6 53.2	88.4	.3 70.4
:	150		67.2 66.8 68.3	68.8 71.7 69.9	69.4 75.9 87.6	78.6 78.4 83.0	79.7 80.7 78.8	78.0 76.1 74.8	73.8 73.3	72.9 71.1 69.7	67.3 65.1 61.4	91.9	.7 78
	140	us	67.0 66.5 69.0	72.0 73.0 72.4	70.5 78.0 87.9	81.1 81.4 86.0	84.0 85.7 83.7	82.8 80.7 78.2	77.8 77.1 74.5	75.9 75.0	70.3 67.4 63.4	94.6	•5 83
	130	R RADI	67.5 65.8 67.2	69.3 72.8 71.9	70.5 77.7 88.1	81.8 80.0 85.8	88.0 89.0 0	82.5 80.9 79.0	77.3 77.3 75.7	74.9 75.7	72.0 68.0 64.3	94.5	\$6 85
	120	5-METE	66.3 65.3 65.9	67.1 71.3 71.4	67.8 75.0 88.8	80.7 77.5 82.2	80.4 82.0 79.4	77.6	73.6 72.3 70.0	71.7 70.3 68.1	66.4 63.5 59.1	92.4	.1 84
	110	ON 30.	67.2 65.2 65.5	69.5 74.2 72.2	69.2 75.2 89.1	81.1 78.9 83.2	80.8 82.0 79.8	78.3 76.9 75.2	74.6 73.0 71.9	72.7 71.6 69.5	67.7 63.9 59.6	92.9	VEL S
	100	(ISPL)	66.8 63.8 66.0	70.7 73.3 70.5	68.2 73.9 86.4	79.6 77.2 82.0	78.7 79.7 77.8	75.8 73.9 72.7	72.0 70.3 68.9	69.7 68.8 65.9	64.2 60.7 57.1	90.8	1SE LE
E, DEG	06	LEVEL	66.3 63.0 65.8	68.5 71.0 70.2	68.7 72.4 86.6	78.5 75.5 81.8	77.5	73.7 72.1 70.3	69.5 68.1 66.2	67.2 66.1 64.4	61.9 57.4 53.1	0.06	IVED NO
ANGL	80	SSURE	68.2 63.7 64.7	67.5 71.3 70.2	70.2 71.7 83.6	77.0	76.2 76.7 74.5	72.2 70.2 68.0	67.0 66.0 63.7	62.5 62.1 59.7	56.9 53.0	88.1	PERCE
	70	NO PRE	69.0 63.3 67.5	68.0 70.8 69.5	68.2 71.7 85.2	77.0 74.9 79.7	75.7 76.0 74.3	72.7 70.4 69.5	68.6 67.1 65.0	66.0° 64.6 62.2	59.6 55.7 51.2	88.7	EL INE
	09	ND SCUN	68.2 63.5 69.0	68.5 71.3 70.4	68.5 73.9 87.1	79.3 76.5 80.3	77.5 78.2 77.0	76.2 74.6 72.8	72.3 71.1 69.5	70.5 68.8 66.9	64.7 61.1 56.0	90.6	S10
	90	AVE BA	68.2 65.0 66.0	67.5 73.5 71.5	69.7 75.0 90.1	81.5 79.2 83.0	80.3 80.7 80.2	79.0 77.6 75.8	74.8 75.1 73.5	72.5 73.0 70.2	68.8 65.0 60.2	93.4	.3 84
	04	/3-0CT	67.8 65.0 67.0	70.2 73.2 72.2	71.576.9	82.8 80.7 85.7	82.5 83.0 81.3	80.5	77.0	75.7 76.1 74.0	72.5 68.3 64.3	95.0	8.8
	30	1	66.0 64.3 66.7	70.5 75.2 74.2	74.2 79.2 90.7	84.5 82.2 85.7	83.7 83.4 82.2	81.3 80.4 78.2	77.8 77.5 75.9	75.0 75.5 72.9	70.5 67.7 63.8	95•3	.7 8I
	20		65.2 64.0 66.3	69.8 75.8 74.7	76.4 81.9 90.4	84.6 82.9 85.7	83.5 84.5 7.2	81.8 80.6 79.0	78.5 77.8 35.9	76.9 76.1	71.7 68.9 64.9	95.5	11 0.
	10		65.2 63.0 65.2	72.37	92.5	80 80 80 4 14 4 6 6 6	88 8 7.4.3 6.0.3	86.5 75.4 76.0	77.5	76.2	41.2	9.36	9 10
FRECCENCY			55 63 80	16C 125 16G	200 250 815	24 č 25 č 25 č 25 č	866 1066	16CC 20CC 25CO	4000 8000	630¢ 800¢ 1000¢	1260C 1600C 200C	EVERALU	DISTANCE 152.6 PETER

# TABLE IV. - Continued. FAR-FIELD NOISE OF QF-9 WITH DESIGN NOZZLE

[Data adjusted to standard day of 15° C and 70 percent relative humidity; SPL re 2×10<sup>-5</sup> N/m<sup>2</sup>; PWL re 10<sup>-13</sup> W.]

(b) Percent of design speed, 70; fan physical speed, 1553 rpm; fundamental blade-passage frequency, 388 hertz.

FRECLENCY							/	ANGLE	E, DEG								AVERAGE	1 8
	9	20	30	07	5.0	69	02	80	6	100	011	120	130	140	150	160	۲	LEVEL
	?	3	;			3	2	3							١.		<del>-1</del>	
				/3-0CT	AVE BA	S. ON	GUND PRE	SSURE	LEVEL	(ISPL)	ON 30	S-METER	R RADIUS	Sn				
35	•	6	•	ė	<b>.</b>	÷.	-			6	8	80			•	5.	•	17.
	67.9	67.8 58.6	67.3	65.8	69.6	66.99 66.9	65.4	65.6 65.9	65.6 66.2	67.6	66.4 68.4	67.0 67.3	70.1	72.3	71.3	75.8	68.7	116.1
														•			,	
25		٠,	e 4	٠,	-	e, c	•		•	•	÷.	<b></b>		•	•		•	200
160		76.8	76.6	75.0	74.6	73.1	72.6	73.0	74.0	74.5	75.3	75.0	76.0	75.6	73.5	75.7	74.7	122.1
		,		,		(			•					,	•	u	,	ç
350	•		•	•	.,	ئى د	٠. ۲	•	<b>5</b> 4	•		77.6	• 0	• •	•		*	202
318	86.3	• ~	P KU	83.0	83.5	82.0	79.3	77.6	78.1	0	91.8	81.7	82.3	82.5	တ		82.0	129.4
466	9	7.96		94.7	2	•		8		•	4	5	4		•6	•	,	41.
200	•	85.0	85.3	. 4	85.8	81.0	79.1	78.5	80.0	82.1	85.8	82.2	83.8	83.8	80.3		82.4	129.8
063	85.2	85.2	, E	83.7	2.	6	•	7	6	-	2.	5.	· 2	•	•	6	2	30.
		6	•	8	-	5	•	5	•		8	6	•	•	ģ	•	æ	70
1000	نا د د د	86.1	85.8	84.5	83.1	81.0	19.0	79.0	90.6	85.8	84.8		86.8	85.6	80.5	80.7	83.6	31
1250		7.	~	2.	•	<b>.</b>	6	6	ä	9	4.	•	8	•	2.	81.8	•	32.
1960	4	2	٠ĸ	5	4	•		7.	6		83.4	m.	7.	86.9	ij	•	3.	-:
2000	83.6	84.1	84.7	83.9	82.7	0	15.9	75.1	77.1	79.7		81.2	85.7		4.62	77.3	82.0	129.4
2600	•	2	2	2.	۲.	œ	*	3	5	8	ċ	6	9	2.	۲.	•	ċ	27.
23.60	_		-		6	,	4	-	4	7	6	å	÷		•	75.2	•	26.
7004	86.9	81.2	81.5	81.9	80.0	76.7	72.2	71.0	73.4	15.1	77.7	17.6	81.4	80.2	75.4	74.4	79.0	126.4
5000		φ.	5	•	æ			8	-	ů	ġ	ď,	ċ	۲.	5	71.8	÷	25.
,30E9		79.7	8			•	•	•	2	4		•	8	6	5	2.	8	25.
2003	75.1	79.3	78.8	79.3	77.0	74.3	0	67.1	71.5	73.6	75.8	74.8	2.62	78.1	73.8	71.8	78.1	125.5
10000	•	•	÷		•	5	•	<b>.</b>	6	1.	÷	5	٠,	5	5	•	ġ	24.
12560	•			•	2.	•		2.	.0	6	-		•		ċ	-	•	23.
16000	71.2	711.7		71.2	68.8	ŝ	<b>60.4</b>	58.1	63.1	65.7	68.2	67.5	71.9	70.7	68.6	9.49	74.6	122.0
20002	•	• '	4.99	•	•	•	•	•	æ		ë.	9	ě	•	•	•	m	20.
CVERALL	5.5	8.66	100.9	98.3	99.5	91.9	6.46	95.0	95.9	94.9	97.3	98.1	98.9	99.3	94.1	93.9	97.6	145.0
DISTANCE	_	}				SID	EL INE	PERCEIV	VED NOT	SE L	EVELS							
152.5 PETER	74	.3 82	7 87	98 6.	.3 90	06 6.	4.	.1 85	98 99	.7 89	16 0.	06	.7 90	.5 88	.9 81	.1 76.	י ניי	_
Na. 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2			<u>`</u>															

(c) Percent of design speed, 86; fan physical speed, 1902 rpm; fundamental blade-passage frequency, 475 hertz

FRECLENCY								ANGE	E, DEG								AVERAGE	0.W
	21	20	30	0,4	50	99	0,	80	06	100	110	120	130	140	150	160	a.	(PWL)
			1	/3-0CT	AVE BA	ND SCUN	D PRE	SSURE	LEVEL	(ISPL)	ON 30.	5-METEI	R RADI	ns				
263	71.8	67.8	70.1	70.3	71.8	72.1	72.9	73.4	73.3	74.6	75.4	73.0	75.1	76.1	77.4	78.1	74.0	121.4
	•	•	6	8	ċ	•	÷	μ.	•	3.	4	•	•	•	•	ċ	4	21.
		9	8	10	3			· 03	S.	8	8	-	6	6	·	o.	٠,	24.
125 160	75.5	82.6 79.8	79.8	79.0	78.0	77.1	77.0	79.1	79.0	80.6	82.1 79.8	79.9	81.8 80.1	80.8	81.0 79.1	79.7	78.8	127.6
U	-	. 2	ö	6	7	•	•	5	5.	•	•	9	•	8	8		-	25.
25C 315	85°C	86.7 87.9	86.3	82.3 84.6	81.3 81.9	79.5	78.0	79.8 80.3	80.5 81.1	81.8 82.3	83.5 84.1	81.9	83.8 84.3	83.2 84.1	80.8	78.9	82.0	129.4
466		2	64	•	Ġ	. 9	Š	4	9	æ	6	4		•	Š		6	36.
300	105.7	101.2	103.7	101.4	100.6	95.7	93.9	91.4	95.2	9.16	7.16	8.46	100.1	1.66	94.7	95.8	98.7	146.1
989	ئ	ô	6	•	•	,	5	e.	ທໍ	-	œ	-	•	8	3	;		34.
BC	•	œ.	•	•	7.	5	4	5	•	8	0	œ	=	•	4	2	8	36.
1000	91.3	3	93.3	93.3	92.1	91.1	87.3	88.3	90.3	91.5	93.1	92.9	96.0	94.1	88.3	86.7	92.2	139.6
Š	•	•	ċ	•	•	<b>.</b>	e M	•	ŝ	•	¢.	å	;	•	•	-	8	35
9	٠	o.	-:	0	8	•	ě	4	5	-	6	æ	ě.	·	*		8	36.
2000	4.0	89.9	4 6 6	89.9	88.0	85.4 8.4	82.5	82.7	84.5	86.2	488.4	88.1	91.7	89.2	83.4	80°4 78.6	87.9	135.3
? .	•	•			•	•	•	•	•	•	•	Ď	•	•	•	•	•	•
3150		87.1	87.6	87.9	5	*	81.7	•	81.7	4.		85.65	.,	9	80.7	•	5	33
38	•	84.7	85.6	• •	83.1	80.6	77.4	76.2		80.1	82.7	, -i	85.4	82.4	. 6	73.8	• •	
Š		•	m	•		-		4	6			2.	•	(n)	æ	•	٠ ۾	30.
2008	83.7	84.1	83.8	84.7	81.5	79.5	75.8	74.7	78.3	79.3	81.6	80.8	84.7	82.5	77.2	73.3	83.3	130.7
ဗ		:	Ο.	5	θ.	è	8	2.	æ	9	ċ	æ	2	6	•	ċ	<b>.</b>	29.
2 5C	w.	8	•	•	•	4	•	9	e.	5	æ	7	•		4	8	Ξ.	28.
16000	74.3	75.9	70.0	75.5	72.3 67.6	70.0 64.8	65.8 60.8	65.7	65.4	71.6	74.7	73.7 69.8	73.6	75.5	72.6	66.6 62.2	79.6	127.0
CVERALL	101.0	104.3	105.7	104.2	102.9	99.4	97.4	96.6	0.66	101.0	102:1	100.6	104.6	103.1	98•3	96.4	102.1	149.5
DI S TANCE						\$10	EL INE	PERCEI	IVED NO	ISE LEV	VEL S							
150 & WEITED	19	4	60 6 6	70 0			10			40	70	-	70	0 4	0	107	<u> </u>	
	,				,							`			5			

### FAR-FIELD NOISE OF QF-9 WITH DESIGN NOZZLE LABLE IV. - Continued.

70 percent relative humidity; SPL re  $2\times10^{-5}$  N/m<sup>2</sup>; PWL re  $10^{-13}$  W.] and Data adjusted to standard day of 15° C

AVERAGE SPL 75.3 79.5 83.5 87.8 99.0 90.4 90.6 88.0 87.4 85.5 85.6 85.4 84.1 83.6 81.7 80.1 80.1 81.9 81.5 90 • 1 88 • 7 03.4 85.1 90.1 81.0 515 hertz. 81.6 81.9 82.7 80.2 81.0 80.9 83.0 94.6 84.9 83.8 86.7 83.5 82.0 80.6 79.6 78.5 75.9 76.5 75.5 73.2 70.8 68.3 64.3 83.1 82.4 83.3 98.1 81.1 160 86.8 79.2 80.0 81.4 85.5 86.5 85.0 83.5 82.3 81.6 81.3 80.4 4.66 83.6 80.6 82.4 82.1 83.7 95.4 86.3 76.3 74.5 71.2 81.3 85.2 150 fan physical speed, 2063 rpm; fundamental blade-passage frequency, 95.0 78.1 78.8 79.9 83**.1** 83**.**4 81.8 84.9 88.1 102.3 91.8 91.7 93.5 90.2 87.6 87.0 79.9 77.3 73.5 81.5 85.1 89.8 84.2 84.1 81.7 104.9 140 98.4 (ISPL) ON 30.5-METER RADIUS 90.2 106.5 77.3 77.6 78.9 81.9 83.3 81.5 86.3 94.7 97.2 94.4 90.5 88.6 87.1 87.5 85.4 84.1 80.1 75.9 87.4 93.3 130 7.96 103.1 101.1 100.1 100.5 101.4 102.5 103.3 103.9 88**.1** 98.6 88.0 79.4 76.0 72.2 80.0 82.7 79.1 83.9 86.2 6.06 97.5 90.5 84.0 84.8 83.1 75.7 91.7 91.6 120 97.2 80.5 76.9 72.2 74.7 73.5 75.5 81.1 83.0 85.8 79.5 88.3 97.3 91.0 92.0 88.6 87.0 85.2 85.3 86.4 91.5 90.1 89.2 110 SIDELINE PERCEIVED NOISE LEVELS 79.7 82.0 81.8 87.6 97.8 91.0 87.1 85.6 78.3 75.1 74.5 78.5 83.3 85.9 91.7 93.5 90.2 88.9 70.7 100 DEG 77.0 72.9 68.4 73.5 73.2 72.0 77.3 81.9 84.0 86.1 97.2 89.0 90.2 92.3 89.0 89.5 87.4 85.3 81.3 82.2 79.3 78.1 81.2 LEVEL 90 ANGLE, 73.0 SOUND PRESSURE 85.0 97.2 87.3 87.9 9.61 78.2 9.49 73.7 77.2 80.2 76.8 80.3 83.4 84.0 83.2 71.8 91.3 88.7 85.7 87.1 80 87.0 84.2 96.9 90.6 80.1 77.8 74.9 72.6 72.3 71.9 76.0 78.8 76.2 80.3 82.0 87.3 85.7 84.9 84.6 82.7 80.2 86.3 63.1 2 94.5 85.5 96.9 87.0 90.3 88.7 87.5 86.8 82.9 83.7 81.4 79.0 77.0 72.2 66.4 72.3 78.2 79.9 80.0 77.6 82.3 83.0 91.5 9 1/3-OCTAVE BAND 78.3 83.0 83.7 86.6 99.1 89.0 88.5 94.5 88.2 87.7 85.2 83.4 78.1 73.6 68.6 73.3 72.2 71.4 79.4 91.7 90.5 89.1 93: 79.7 89.2 20 (d) Percent of design speed, 89.6 89.6 87.9 86.4 85.9 83.5 72.6 72.2 70.5 79.6 81.2 79.0 83.9 85.0 88.2 98.4 90.7 89.5 8.06 93.2 91.6 81.5 76.5 72.0 103.6 40 72.7 73.1 72.2 78.0 83.2 82.0 91.7 100.6 91.8 89.3 88.7 86.6 85.3 85.2 82.0 79.6 75.9 71.4 105.0 81.7 85.3 87.2 91.3 97.0 91.8 91.06 30 91.6 102.9 93.6 79.4 84.0 86.5 88.0 91.4 88.8 88.4 4.86.1 86.3 85.8 82.6 80.1 76.7 71.7 105.8 82.6 95.0 91.1 74.5 20 96.6 101.1 92.1 87.6 87.6 72.8 86.5 65.38 83.5 86.1 94.5 84.8 75.7 75.3 71.8 104.4 8.58 91.3 96.1 EE.4 96.0 86.1 9 DIETANCE CVERALL FRECUENCY 100 5000 63CC 80CC 215C 400C 160 966 160C 200C 250C 1250C 160CC 200CC

135.2 146.4 137.8

138.0 141.7 137.5

139.3 137.5 136.1

135.4 134.8 132.9

126.9 130.9 132.5

122.7 122.9 123.4

POWER LEVEL (PWL)

127.5 129.3 128.9

133.0 132.8 131.5

131.0 129.1 127.5

150.8

97.0

0.96

6.46

94.1

95.0

93.6

92.1

88.8

79.1

152.5 WETERS

(e) Percent of design speed, 100; fan physical speed, 2164 rpm; fundamental blade-passage frequency, 541 hertz.

6 79.4 80.9 82.5 85.6 78.3 6 80.9 85.1 86.1 86.1 86.4 83.0 85.0 85.0 85.0 85.0 85.0 85.0 85.0 85
6 79.4 80.9 82.5 85.6 78. 6 80.5 82.2 83.7 85.9 78. 5 83.5 84.3 85.3 86.5 80. 4 85.1 86.1 86.1 86.4 83. 6 86.9 86.5 86.0 85.6 85.
6 80.5 86.2 85.6 84.9 85.6 85.9 86.5 86.0 85.9 86.2 85.6 84.9 85.
4 85.1 86.1 86.1 86.4 85.6 85.9 86.2 85.6 84.9 85.
6 86.9 86.5 86.0 85.6   85. 6 85.9 86.2 85.6 84.9   85.
1 85.1 84.6 84.2 83.6   83 7 00 7 07 4 04 4 03.6   04
91.2 89.9 86.2 85.1 89.
7 92.9 89.1 85.7 85.1 90
5 97.1 91.1 94.9 98.
6 97.2 93.7 89.3 88.9 94.
3 97.2 94.1 89.1 87.3 93
.0 95.7 90.5 88.9 95.
7 96.2 92.6 88.6 87.1 93.
2 98.2 92.7 87.7 86.1 93.
.6 90.8 86.3 84.
0 94.2 89.7 84.7 82.8 90.
5 93.0 89.4 83.9 81.6 90.
.3 92.5 88.3 83.8 81.1 89.5
0 91.1 86.2 82.0 79.5 87.
5 89.5 87.0 81.2 77.7 87.
.9 90.0 86.2 82.0 78.0 87.9
8 81.9 84.5 80.0 73.7 80.
0 87.0 83.2 80.0 76.0 87.
.1 83.4 80.9 76.2 73.0 85.9 .0 80.9 78.1 74.0 69.4 85.6
.5 108.1 104.4 100.2 100.2 105.1
100.6 100.3 94.1 86.9 82.8

TABLE IV. - Continued. FAR-FIELD NOISE OF QF-9 WITH DESIGN NOZZLE

[Data adjusted to standard day of 15 $^{0}$  C and 70 percent relative humidity; SPL re 2×10 $^{-5}$  N/m $^{2}$ ; PWL re 10 $^{-13}$  W. ]

(f) Percent of design speed, 110; fan physical speed, 2380 rpm; fundamental blade-passage frequency, 595 hertz.

FRECKENCY								ANGL	E, DEG						•		AVERAGE	OWE
	10	20	30	40	50	09	70	80	90	100	110	120	130	140	150	160	Δ.	(PWL)
			1	/3-0CT	AVE BA	ND SCU	ND PRE	SSURE	LEVEL	(SPL)	ON 30.	5-METE	R RADI	ns				,
9 6 6 0 6 9	76.1 75.7 86.4	75.7 76.7 82.5	77.6 75.8 79.2	76.9 75.8 77.4	76.9 75.8 76.7	78.7 76.7 77.9	78.4 77.0 78.2	79.1 76.3 80.0	79.7 77.3 82.0	79.2 77.7 83.0	80.4 80.0 83.9	80.5 80.8 83.8	82.6 82.7 85.5	84.6 85.3 87.2	85.2 86.5 88.7	88.1 88.9 90.6	81.0 80.9 83.6	128.4 128.3 131.0
100 125 160	86 6. 3 2. 4. 4. 4. 4. 4. 4. 4. 4. 4. 4. 4. 4. 4.	89.00 89.00 89.00 89.00	82.6 89.0 88.8	81.6 89.2 86.3	81.4 86.4 87.8	83.1 89.5 86.4	81.8 89.2 87.9	83.3 89.7 87.6	84.3 91.4 89.9	84.6 90.5 90.6	86.9 93.0 91.6	87.4 92.8 93.4	88.3 91.9 91.8	89.3 92.0 90.3	89.8 90.9 89.1	89.5 89.1 89.6	85.8 90.7 89.9	133.2 138.1 137.3
260 250 315	96.54	89.6 90.0 91.9	88.1 89.9 91.7	84.8 89.0 90.0	84.8 87.7 89.2	84.3 89.4 89.2	83.8 87.5 89.9	84.3 87.7 90.5	84.4 89.0 92.0	85.9 90.5 93.7	86.9 91.0 94.0	88.4 92.3 93.1	88.6 92.5 93.5	88.3 91.2 91.2	87.3 89.0 87.9	87.2 87.8 86.9	86.5 90.0 91.7	133.9 137.4 139.1
4 R 0	51.2 91.8 96.1	93.4 93.7 101.2	93.0 93.7 102.1	89.9 95.5 105.6	90°2 92°5 98°6	89.5 93.2 101.7	90.4 92.7 99.7	91.4 95.5 104.1	93.0 96.5 104.6	94.7 97.3 105.7	95.5 97.5 105.2	95.8 98.1 106.5	96.5 98.3 106.4	93.2 94.7 100.7	89.4 91.2 97.7	88.2 90.6 97.3	93.3 95.8 103.9	140.7 143.2 151.3
86C 106C 1250	85.8 85.7	91.3 91.5 94.4	91.1 91.6 95.4	91.6 91.4 95.5	91.3 90.2 93.0	91.0 91.0 93.4	93.1 92.4 95.0	94.8 93.9 95.2	96.8 96.5 97.7	98.8 98.5 100.5	99.0 99.2 101.5	99.5 99.5 100.6	100.3 99.6 105.0	97.0 95.5 97.9	91.8 91.2 92.4	90.5 90.6 91.9	96.5	143.9 143.6 146.4
1 6 C C 2 5 C C C C C C C C C C C C C C C C	8 8 8 8 2. 2. 3 8 . 5	90.9 91.1 89.7	91.3 91.6 90.2	91.6 92.1 90.7	90.4 91.1 89.5	90.9 90.6 89.2	90.9 90.6 89.2	92.9 -92.3 90.4	95.1 94.8 92.9	96.8 96.4 95.1	98.6 58.4 96.7	99.9 99.0 97.7	100.6 101.3 98.2	94.4 94.6 92.9	90•3 90•6 88•5	88.7 88.7 86.8	95.9 95.9 94.1	143.3
215 4000 5000	0 0 0 0 0 0 0	88.1 88.1 86.5	89.0 88.6 86.5	89.9 89.6 88.1	88.0 88.0 85.8	88.9 87.5 84.5	88.5 87.1 84.8	88.9 86.3 6.5	91.9 91.3 88.8	94.7 93.0 91.0	96.2 94.5 93.2	96.5 95.4 93.0	96.7 96.6 94.8	92.2 92.1 89.8	87.9 88.1 86.3	85.1 84.9 83.6	93.4 92.7 91.0	140.8 140.1 138.4
63CC 60CC 1000C	82.0 83.0 83.0	85.6 85.4 83.0	85.1 84.8 81.7	8 8 8 5 6 7 8 7 8 7 8	83.5 82.8 79.7	85.5 83.5 81.9	85.0 82.8 80.2	84.8 84.1 82.2	87.8 88.3 85.5	91.5 89.6 87.5	93.0 91.8 89.7	93.8 92.0 89.9	93.3 94.0 92.2	91.1 89.8 88.2	85.3 86.2 84.0	82.2 82.0 79.5	91.2 91.3 89.9	138.6 138.4 137.3
125CC 16CGC 2CGCC	76.2	81.3 78.3 74.8	75.8 77.2 73.7	82.1 77.8 74.5	78.6 74.6 70.5	80.4 76.5 72.8	79.1 75.8 72.2	81.1 77.0 74.5	84.6 80.7 78.2	86.3 83.3 80.2	88.1 85.2 81.5	89.1 85.7 82.6	90.9 87.0 84.2	86.8 84.4 81.4	83.8 80.0 77.5	79.8 76.9 73.0	90.1 88.6 88.2	137.5 136.0 135.6
CVERABL	102.4	105.5	105.9	107.7	103.6	105.0	104.5	107.1	108.5	110.0	110.6	1111.3	112.3	107.4	104.0	103.3	1.38.7	156.1
DISTANCE	_   '					SI	EL INE	PERCE 1	VED N	ISE LE	VELS							
152.5 METE	RS 77	88 6	•5 93	1.3 97	96 99	.7 98	•4 98	•5 101	•6 103	.2 104	•6 104	.7 104	.7 104	76 9.	• 4 91	.1 85.	<del>-</del>	

(g) Percent of design speed, 115; fan physical speed, 2488 rpm; fundamental blade-passage frequency, 622 hertz.

TABLE IV. - Concluded. FAR-FIELD NOISE OF QF-9 WITH DESIGN NOZZLE

[Data adjusted to standard day of  $15^{\rm o}$  C and 70 percent relative humidity; SPL re  $2 \times 10^{-5} \, {
m N/m}^2$ ; PWL re  $10^{-13} \, {
m W.}$  ]

(h) Percent of design speed, 120; fan physical speed, 2596 rpm; fundamental blade-passage frequency, 649 hertz.

, , ,	/					-		ANGL	E, DEG								AVERAGE	2 U.
	10	50	30	40	50	09	70	80	06	100	110	120	130	140	150	160	ν.	(PWL)
	`		1	/3-0CT	AVE B	AND SCUNE	) PRE	SSURE	LEVEL	(3PL)	ON 30.	S-METE	R RADI	Sn				
7 40 80 7 40 70	8 1- 8 12 1- 8 12 1- 8	82.3 78.8 87.3	82.3 78.2 88.9	84.3 77.7 85.6	80.0 77.2 83.1	84.3 77.3 81.4	84.3 78.5 79.4	82.6 78.5 82.1	84.5 78.8 81.9	85.6 79.5 82.4	81.8 80.3 85.4	84.1 82.4 87.0	84.6 84.8 90.4	88.5 87.2 90.8	88.0 88.7 90.9	90.7 90.9 93.7	84.9 82.7 86.9	132.3 130.1 134.3
100 125 160	86.9 92.9 93.6	88.8 94.9 94.1	88.6 94.3 92.8	87.3 94.6 91.3	85.9 90.8 90.3	85.1 89.4 90.6	85.1 90.4 91.0	85.4 91.4 91.3	85.3 91.6 92.3	86.9 92.4 93.3	88.4 93.6 94.0	89.2 94.2 95.6	90.4 94.8 94.1	91.7 94.1 93.3	90.9 92.4 90.8	91.6 91.0 90.3	88.2 92.8 92.7	135.6 140.2 140.1
2CC 25C 315	92°5 94°1 94°2	96.7 95.0 95.2	93.5 93.6 95.4	89.5 93.3 94.5	89.2 92.3 93.0	88.2 90.8 93.0	87.0 89.8 93.2	88.8 91.1 94.4	88.5 92.8 95.0	90.0 94.5 96.7	91.0 96.1 97.2	92.1 96.9 97.8	92.5 97.0 97.2	91.7 95.0 95.0	90.2 91.3 91.7	90°4 90°2 90°2	90.8 94.0 95.3	138.2 141.4 142.7
400 500 500	0 - 1 6 6 - 3 6 6 - 3 6 6 - 3 6 7 6 6	94.9 94.6 103.0	95.6 95.1 101.0	94.6 95.4 101.6	94.4 94.6 100.6	93.9 94.8 99.6	93.8 -95.9-	95.4 97.8 107.6	97.4 98.9 108.8	99.8 100.3 108.3	101.1 100.6 105.5	101.9 101.5 109.6	101.1 100.9 110.8	97.8 97.4 105.1	93.6 93.9 102.6	91.8 92.8 96.5	98.1 98.4 106.6	145.5 145.8 154.0
8CC 10CC 1250	92.6	94.7 93.9 96.6	95.2 95.0 99.2	95.4 95.1 97.6	95.6 94.4 97.4	95.2 95.2 96.9	97.9 96.4 97.9	100.0 98.4 100.2	101.5 100.2 101.2	102.7 101.6 102.7	102.9 102.7 104.1	103.6 103.2 104.3	104.4 103.9 105.2	100.7 99.1 101.4	96.2 95.1 96.4	94.6 94.1 95.5	100.7 99.9 101.5	148.1 147.3 148.9
1866	91.7 92.7 9C.1	92.9 94.8 92.1	94.0 95.0 92.6	93.7 95.3 93.6	93.5 94.3 92.0	93.7 94.5 91.8	94.7 94.7 92.8	96.9 95.8 94.3	99.2 98.8 96.8	100.5 100.7 99.3	101.9 102.3 100.6	103.5 103.1 101.7	104.9 104.7 102.5	98.5 98.5 96.6	94.2 94.5 92.6	92.4 92.4 90.4	99.6 99.7 98.0	147.1
215C 40CC 50CC	8.5.0 9.5.0 0.1.0 0.1.0	91.3 91.2 88.6	91.8 91.4 89.0	92.1 92.1 91.1	91.1 91.2 88.6	91.9 91.2 88.5	92.4 90.5 88.5	93.6 93.0 91.0	95.9 95.6 94.0	98.9 97.2 95.3	100.3 99.0 98.2	101.2 100.4 98.2	101.4 101.9 100.7	96.8 96.7 94.7	92.1 91.9 91.2	89.2 89.0 88.3	97.6 97.2 95.9	145.0 144.6 143.3
63CC 60CC 100CC	0 0 0 0 0 0 0 0 0	87.8 87.7 85.2	87.8 87.2 84.1	88.6 88.0 85.7	86.5 85.7 83.0	89.0 87.5 85.7	89.2 87.2 84.5	89.2 89.0 86.7	92.5 92.9 90.3	95.8 94.3 92.0	98.0 96.7 94.8	98.9 97.2 95.6	99.2 99.8 97.8	96.5 95.3 93.7	90.3 91.3 89.5	86.7 86.9 84.6	96.0 96.0 95.0	143.5
125CC 16CC 2000C	81.1 77.5 74.1	83.6 80.4 76.6	82.3 79.7 75.4	84.4 79.9 76.2	81.6 77.4 73.6	84.3 80.2 76.4	83.3 80.0 76.4	85.6 81.4 79.0	89.3 85.2 82.6	91.0 87.4 84.4	93.3 90.2 86.2	94.4 91.0 88.0	96.8 92.9 89.7	92.1 89.7 86.6	88.8 85.4 82.9	84.7 81.6 77.5	95.2 93.6 93.1	142.6 141.0 140.5
CVERAL	105.5	108.2	107.9	107.7	106.8		108	6.0	12.4	113.2	113	115.1	116.0	1111.4	107.9	105.7	112.2	159.6
DISTANCE 152.5 METER	27	4 91	2 94	76 6.	86 88	-	.1 102	7 10	7 4	135	>   ~	108	1.6 108	.3 101	.5 95	.3 87.	- 1 <del>o</del>	

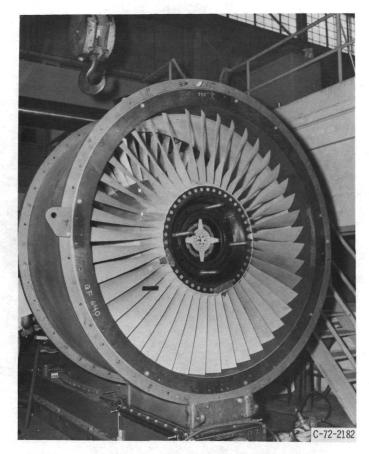


Figure 1. - View of QF-6 rotor blading.



Figure 2. - View of QF-6 stator blading.

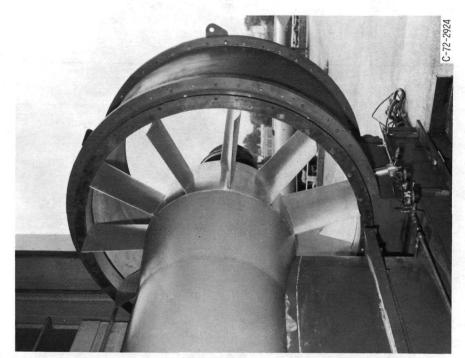


Figure 4. - View of QF-9 stator blading.



Figure 3. - View of QF-9 rotor blading.

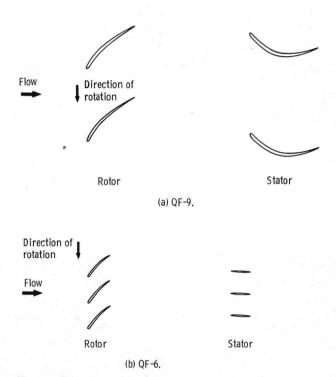


Figure 5. - Relative blade positions for QF-6 and QF-9. All cross sections at tip location viewed inward toward hub.

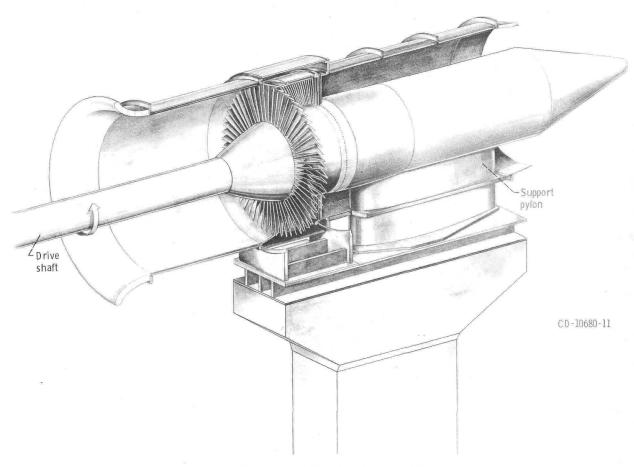


Figure 6. - Cutaway sketch of typical fan installation.

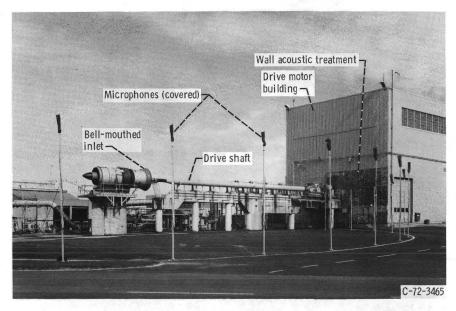


Figure 7. - Test site showing QF-9 in place.

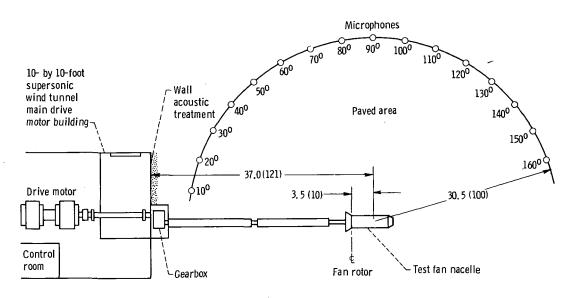


Figure 8. - Plan view of quiet-fan acoustic test facility. (All dimensions are in m (ft).)

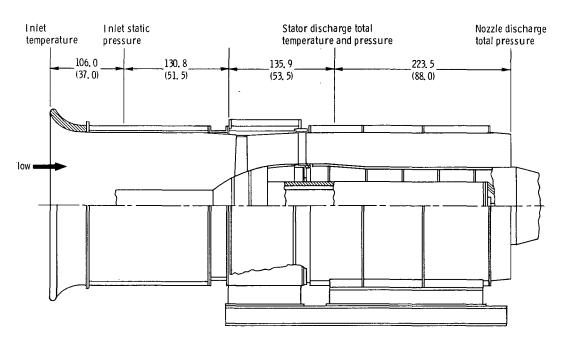


Figure 9. - Cross section of QF-6 fan stage (hard walls). (All dimensions are in cm (in.), )

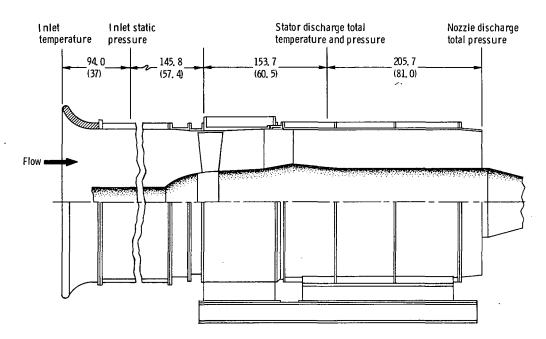
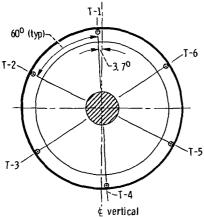


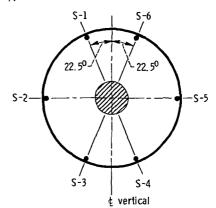
Figure 10. - Cross section of QF-9 stage (hard walls). (All dimensions are in cm (in.).)

### Instrumentation

- O Total pressure element
- ⊕ Total temperature element, T
- Static pressure tap, S



Temperature at lip of bell-mouthed inlet.



Inlet static pressure taps.

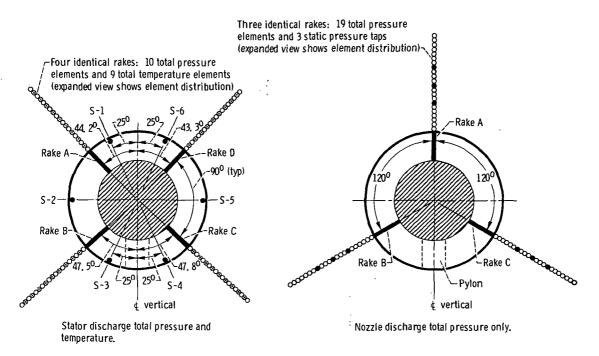


Figure 11. - Detail of fan aerodynamic instrumentation. All views looking downstream. Instrumentation common for QF-9 and QF-6.

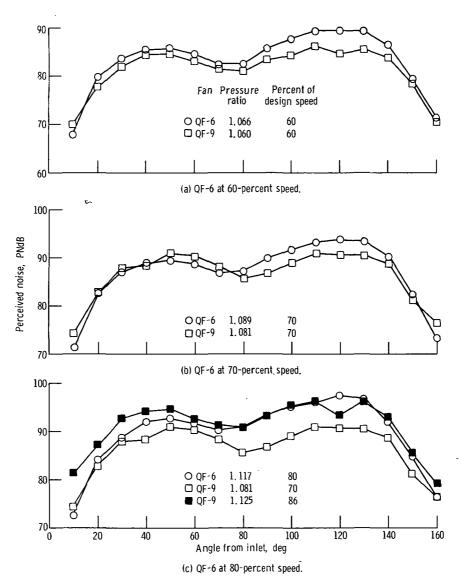


Figure 12. - Perceived noise on a 152.5-meter (500-ft) sideline.

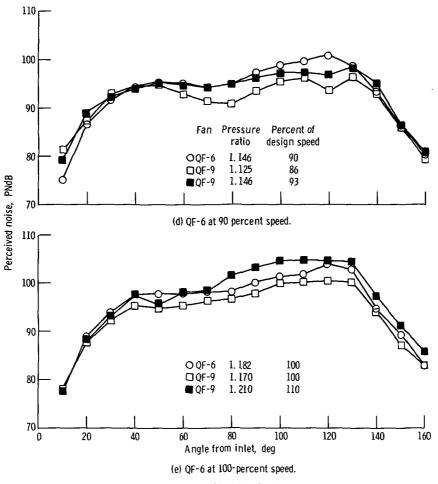


Figure 12. - Concluded.

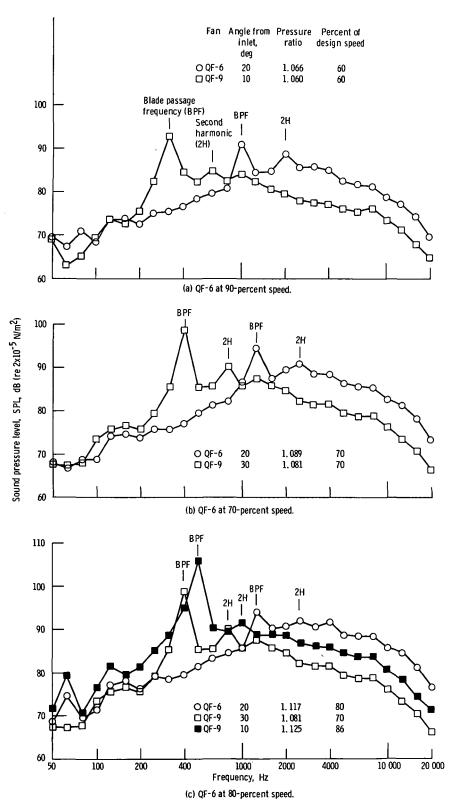


Figure 13. - Sound pressure level at maximum-intensity angle on a 30.5-meter (100-ft) radius - front-quadrant 1/3-octave spectra.

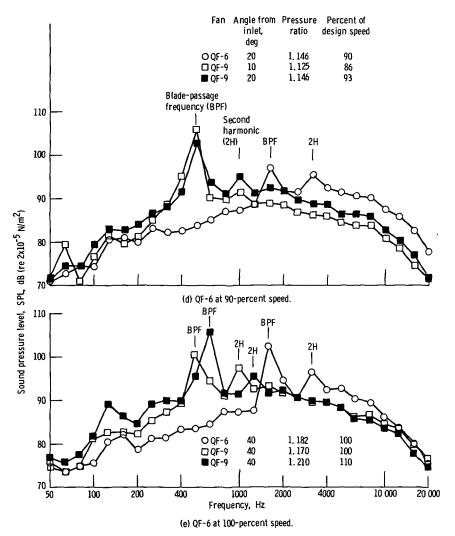


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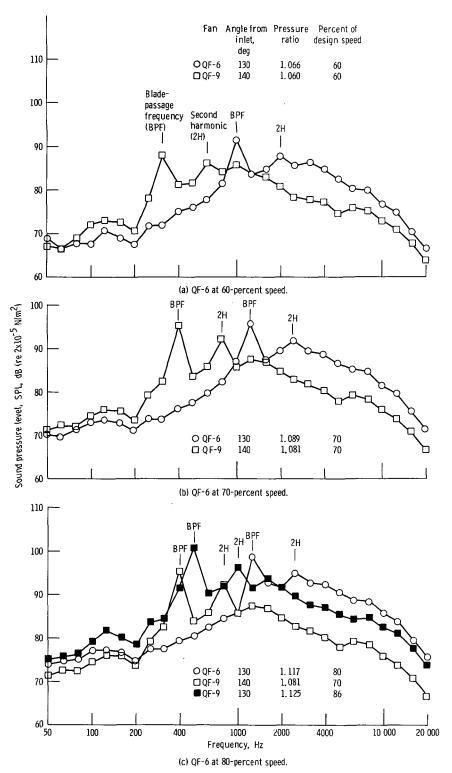


Figure 14. - Sound pressure level at maximum-intensity angle on a 30.5-meter (100-ft) radius rear-quadrant 1/3-octave spectra.

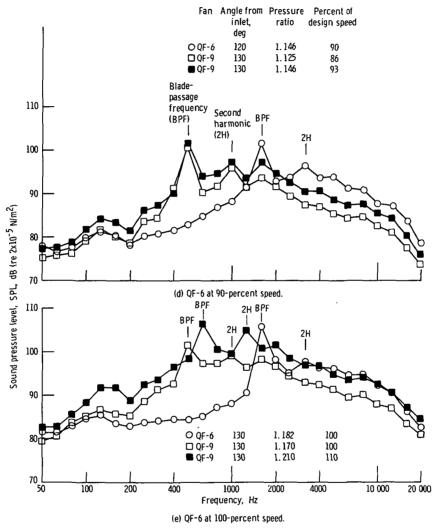


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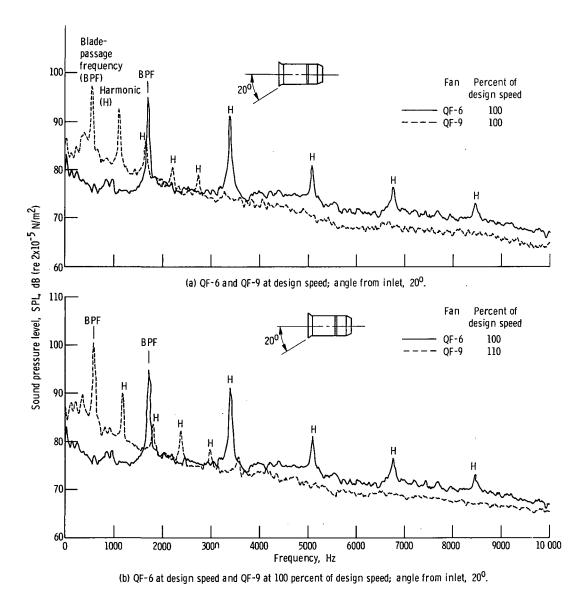
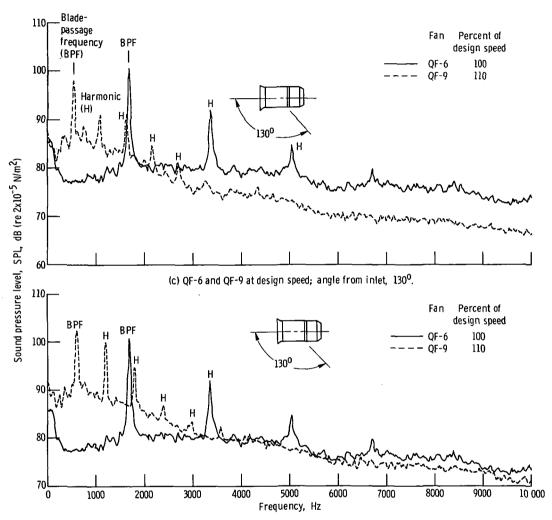


Figure 15. - Comparison of QF-6 and QF-9 narrow-band spectra. Bandwidth, 32 hertz; both fans in design configuration.



(d) QF-6 at design speed and QF-9 at 110 percent of design speed; angle from inlet, 130°.

Figure 15. - Concluded.

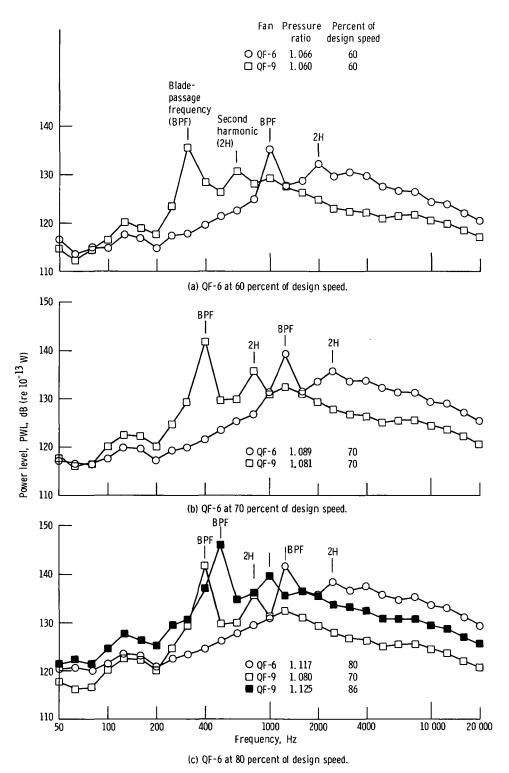


Figure 16. - Power level comparison - 1/3-octave spectra.

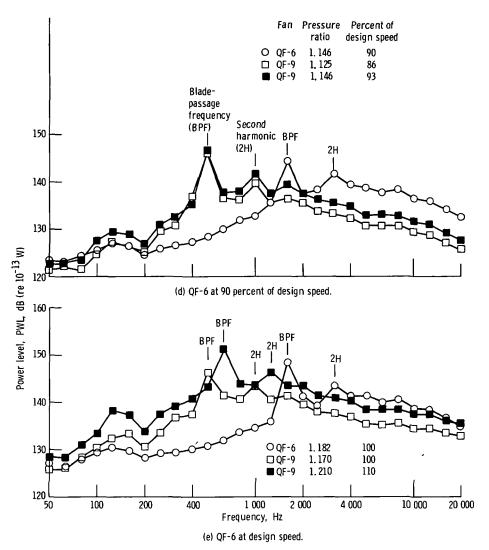


Figure 16. - Concluded.

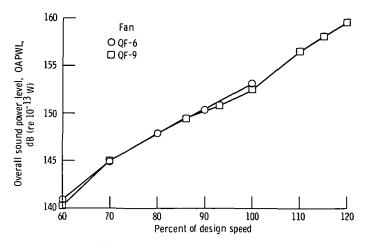


Figure 17. - Overall power level as function of percent of design speed.  $\,$ 

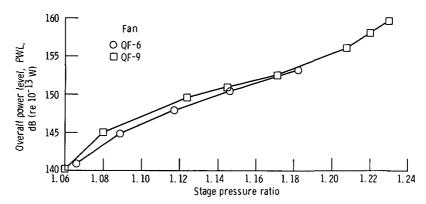


Figure 18. - Overall power level as function of stage pressure ratio.

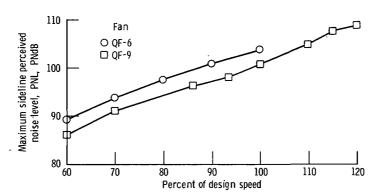


Figure 19. - Maximum perceived noise level on 152. 5-meter (500-ft) sideline as function of percent of design speed.

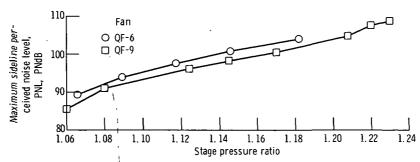
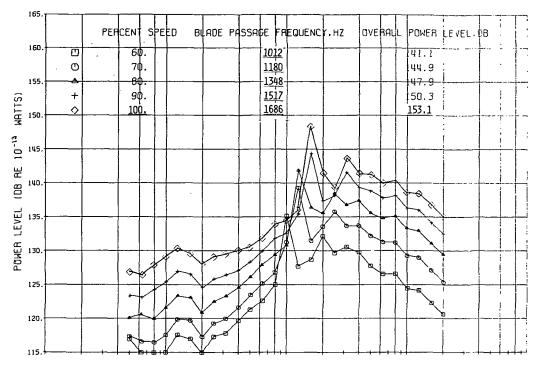
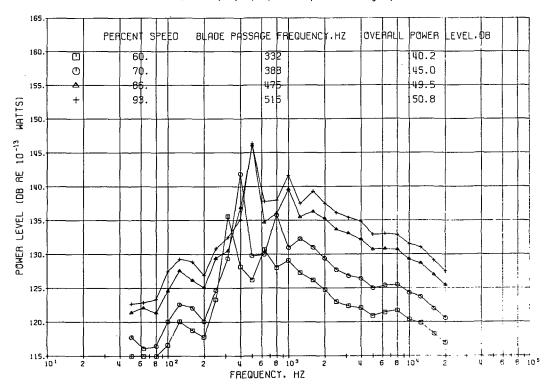


Figure 20. - Maximum perceived noise level on 152.5-meter (500-ft) sideline as function of stage pressure ratio.

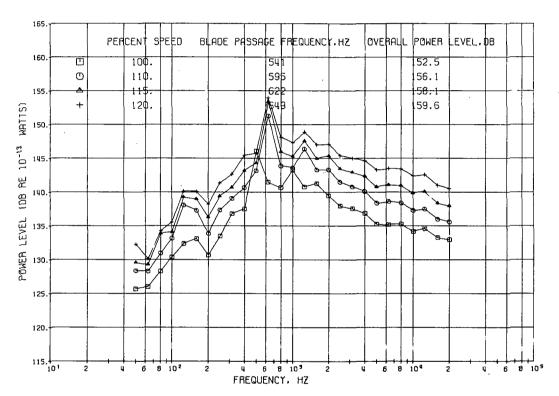


(a) QF-6 at 60, 70, 80, 90, and 100 percent of design speed.



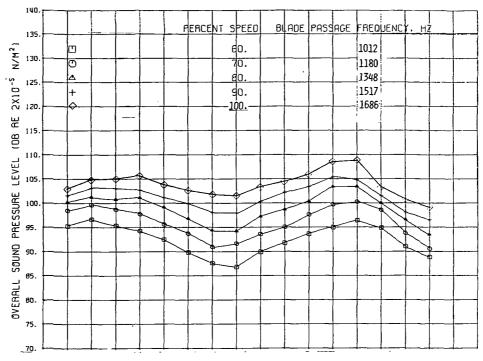
(b) QF-9 at 60, 70, 86, and 93 percent of design speed.

Figure 21. - Comparison of power spectra for QF-6 and QF-9 at various speeds.

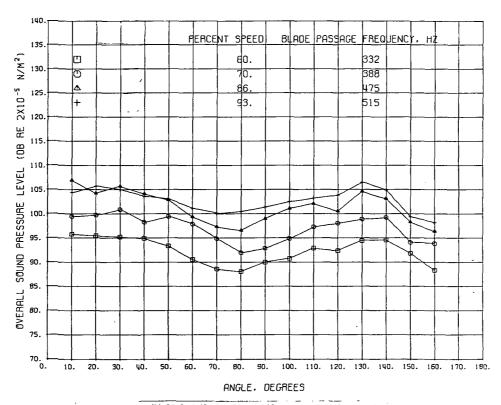


(c) QF-9 at 100, 110, 115, and 120 percent of design speed.

Figure 21. - Concluded.

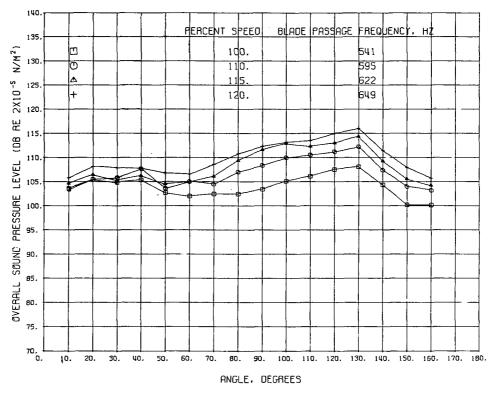


(a) QF-6 at 60, 70, 80, 90, and 100 percent of design speed.



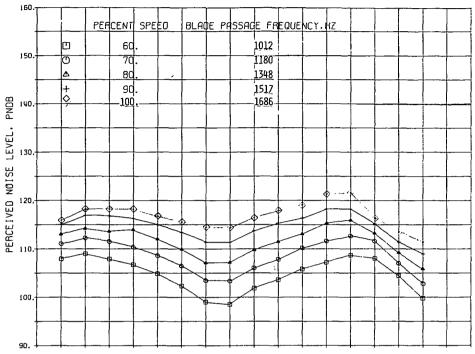
(b) QF-9 at 60, 70, 86, and 93 percent of design speed.

Figure 22. - Overall sound pressure level as function of angle on 30.5-meter radius.

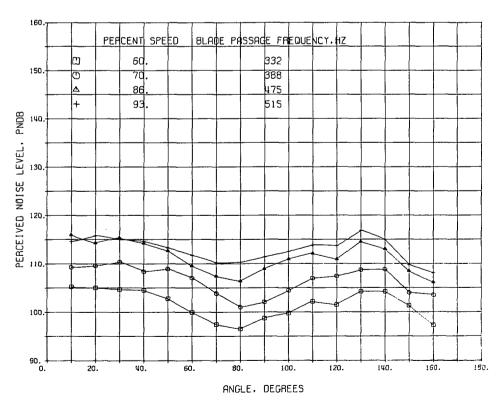


(c) QF-9 at 100, 110, 115, and 120 percent of design speed.

Figure 22. - Concluded.

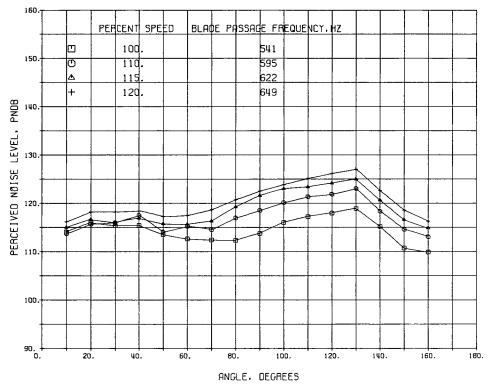


(a) QF-6 at 60, 70, 80, 90, and 100 percent of design speed.



(b) QF-9 at 60, 70, 86, and 93 percent of design speed.

Figure 23. - Perceived noise on 30.5-meter radius.



(c) QF-9 at 100, 110, 115, and 120 percent of design speed. Figure 23. - Concluded.

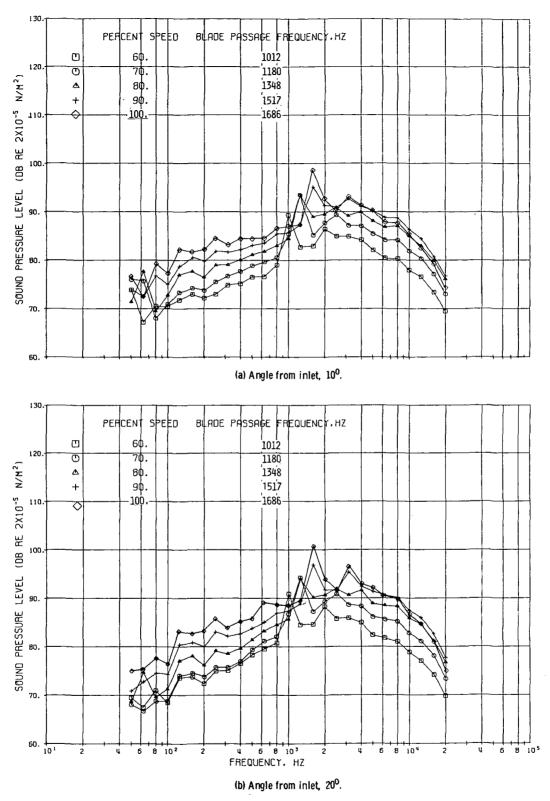


Figure 24. - One-third-octave-band spectra on 30.5-meter radius for QF-6 at 60, 70, 80, 90, and 100 percent of design speed, for various angles from the inlet.

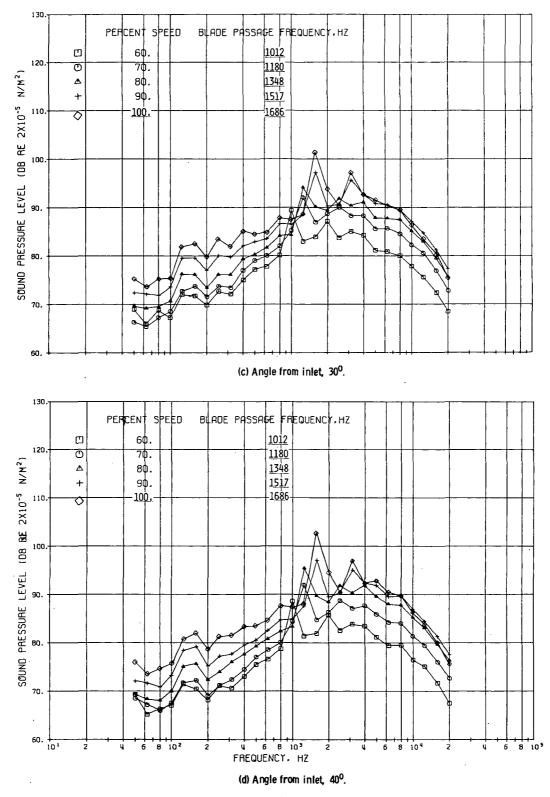
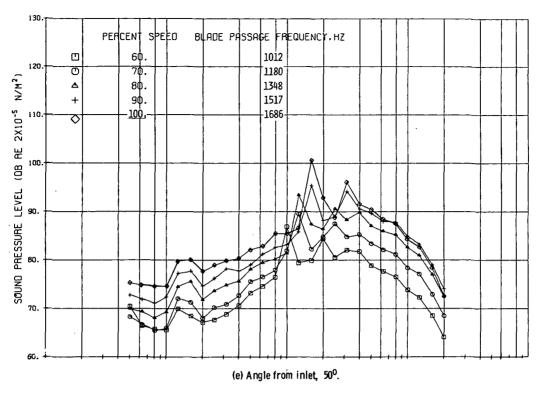
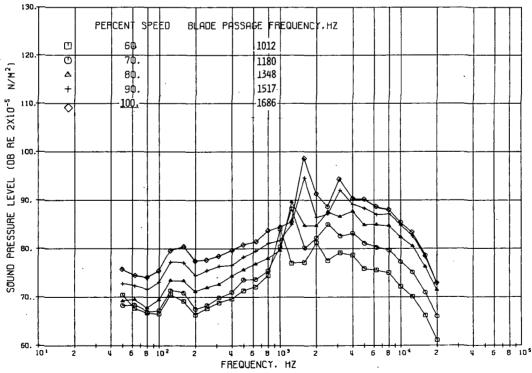


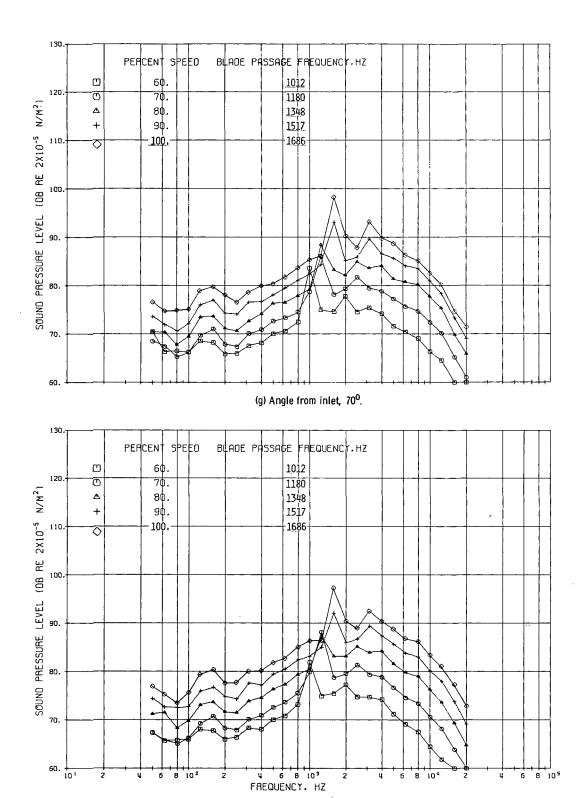
Figure 24. - Continued.





(f) Angle from inlet,  $60^{\circ}$ .

Figure 24. - Continued.



(h) Angle from inlet, 80°. Figure 24. - Continued.

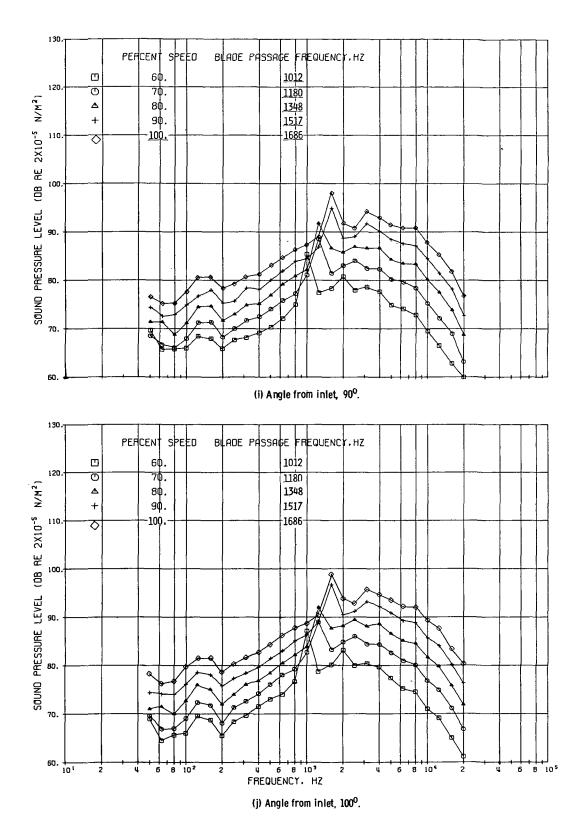


Figure 24. - Continued.

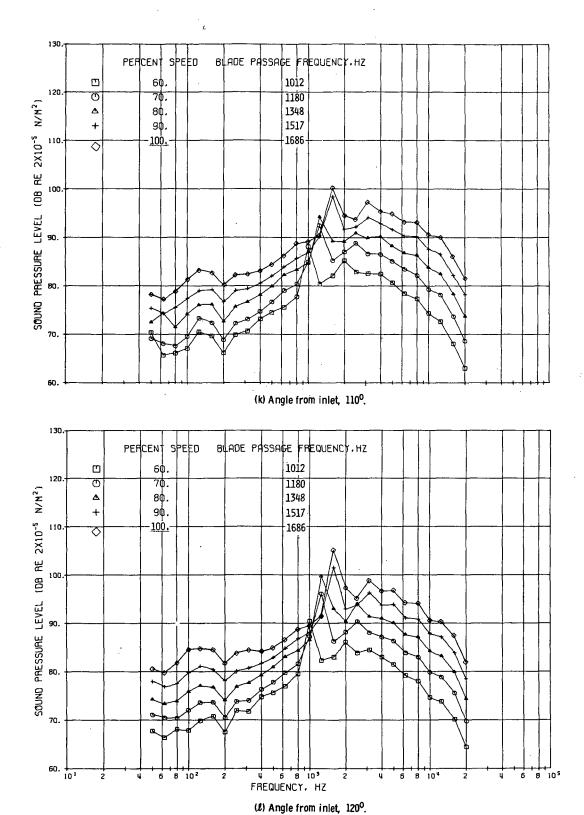


Figure 24. - Continued.

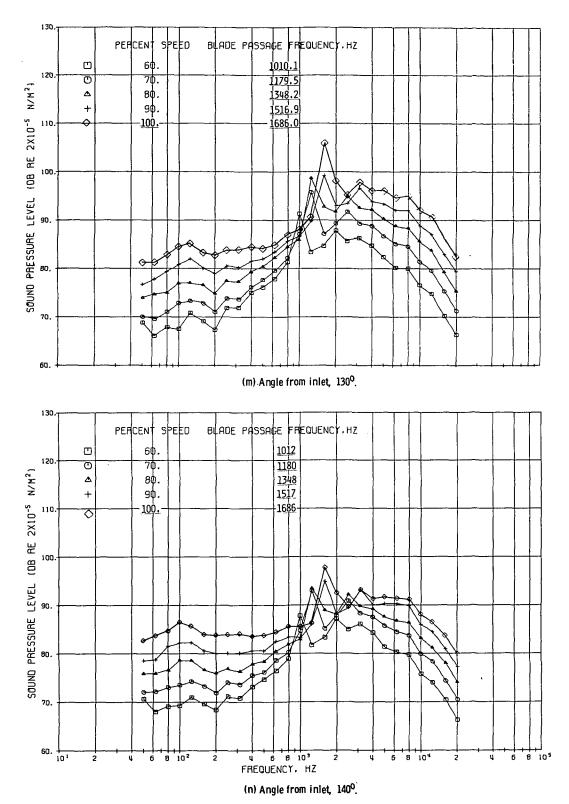


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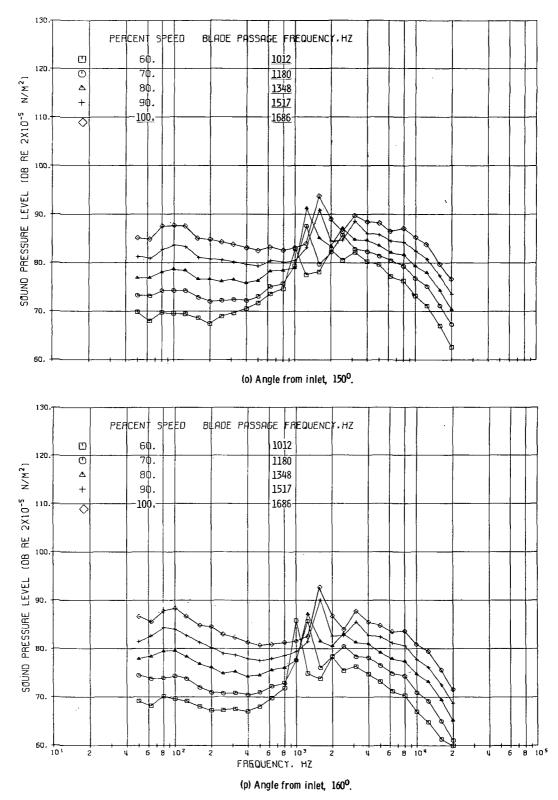


Figure 24. - Concluded.

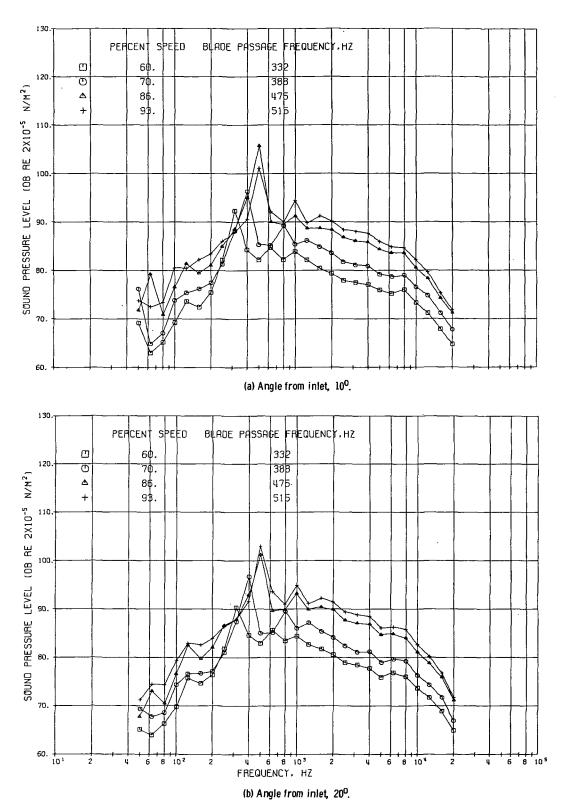


Figure 25. - One-third-octave-band spectra on 30.5-meter radius for QF-9 at 60, 70, 86, and 93 percent of design speed, for various angles from the inlet.

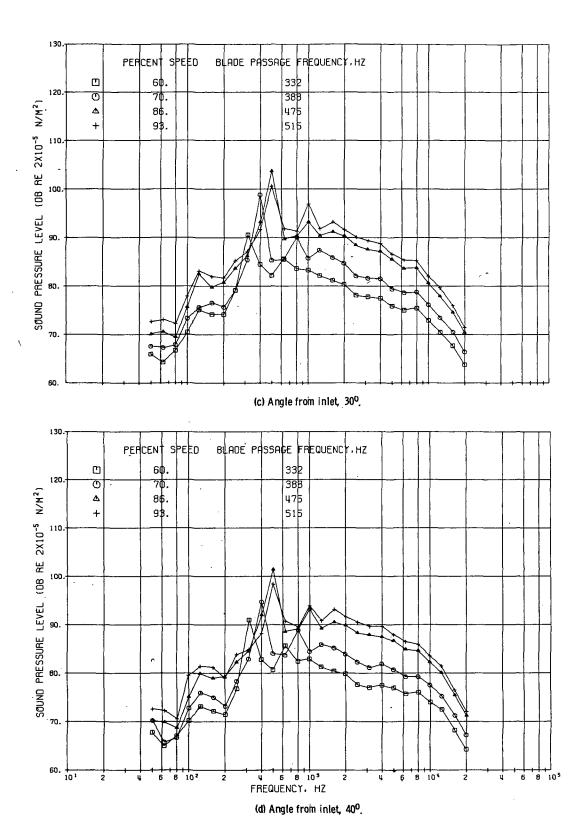


Figure 25. - Continued.

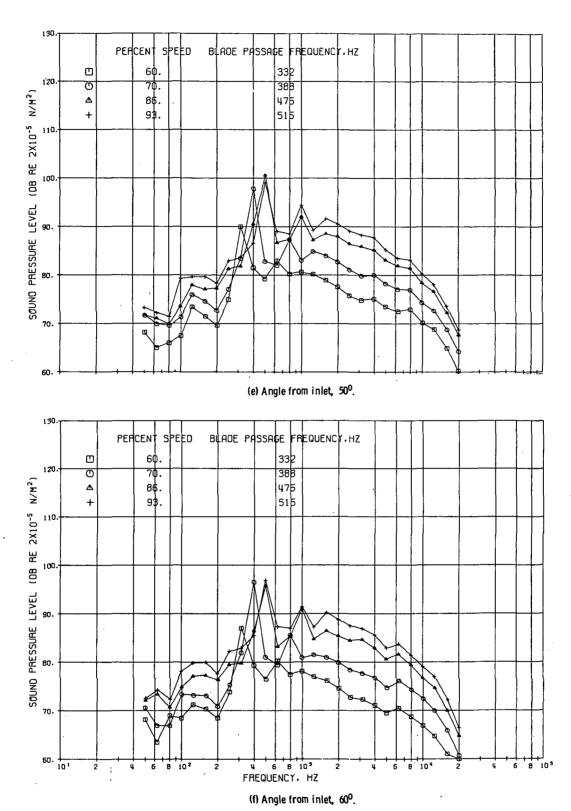


Figure 25. - Continued.

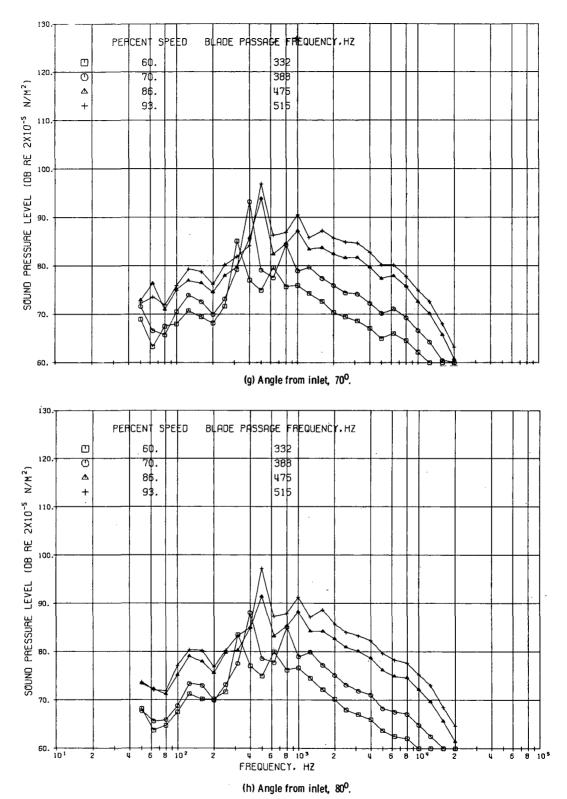
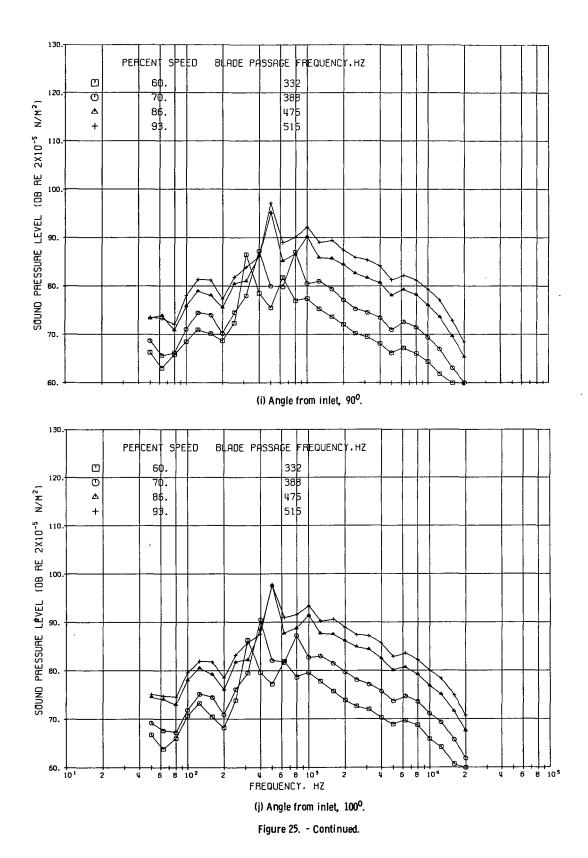


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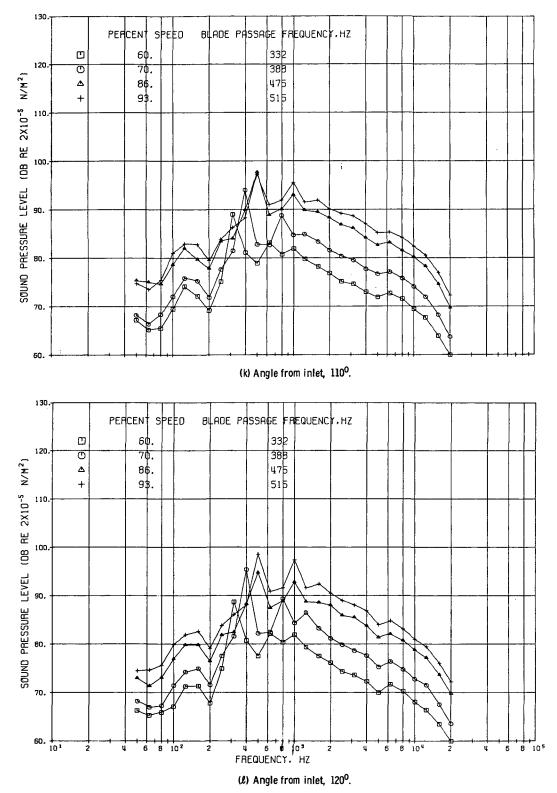


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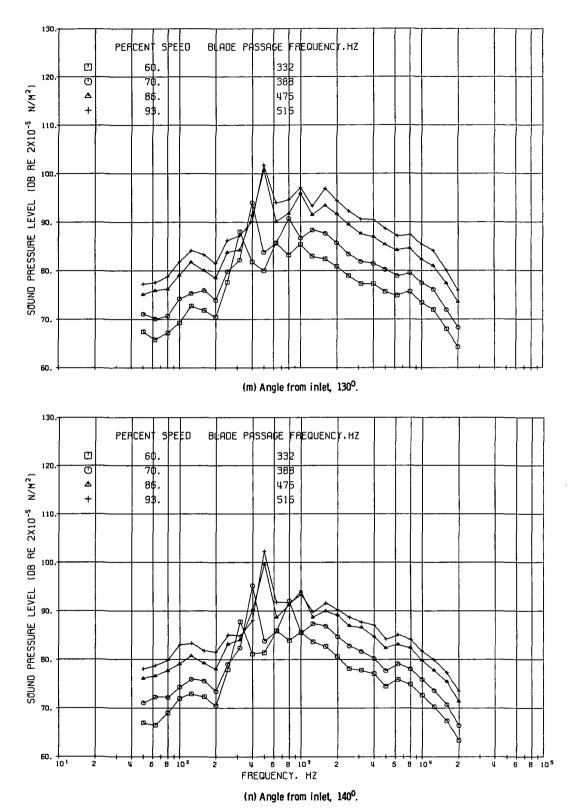


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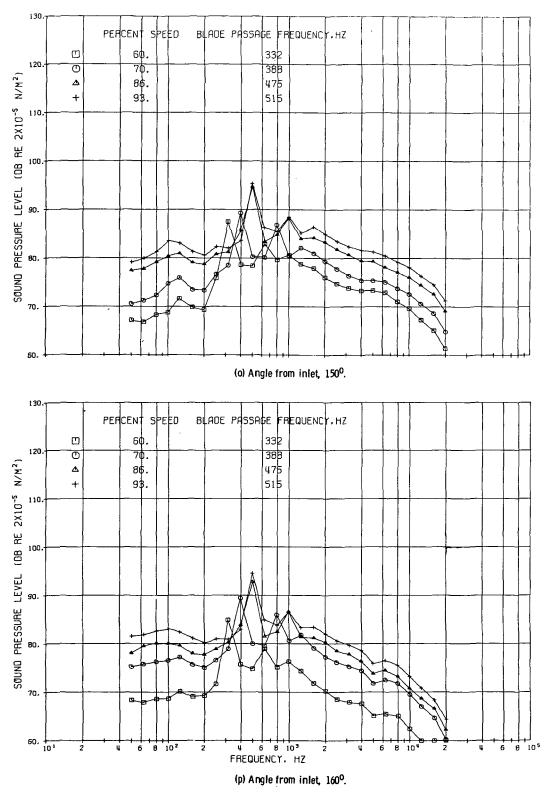


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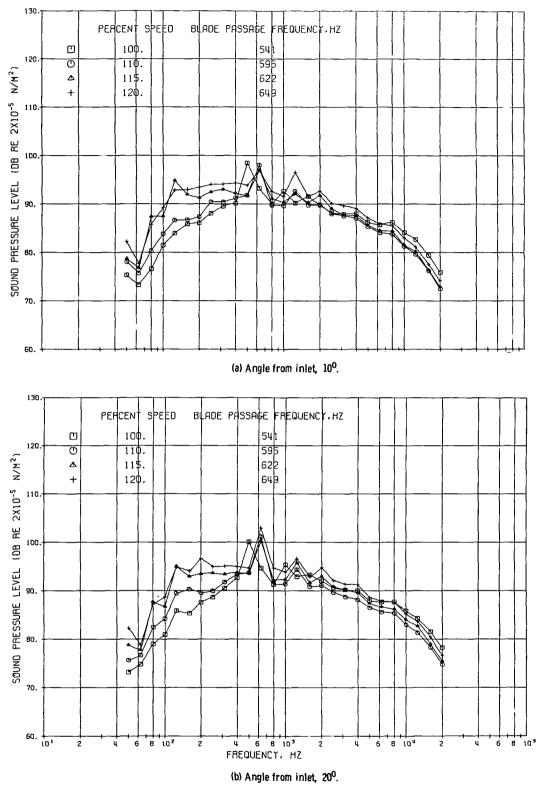


Figure 26. - One-third-octave-band spectra on 30.5-meter radius for QF-9 at 100, 110, 115, and 120 percent of design speed, for various angles from the inlet.

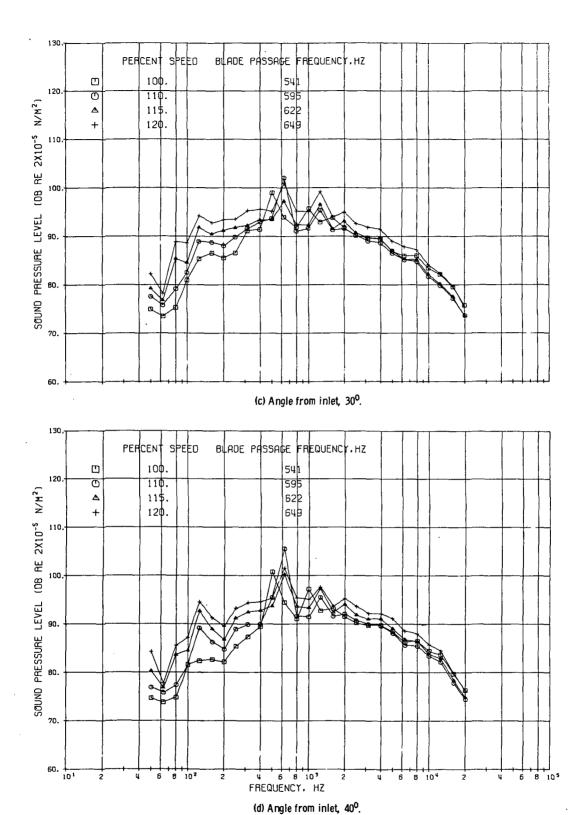


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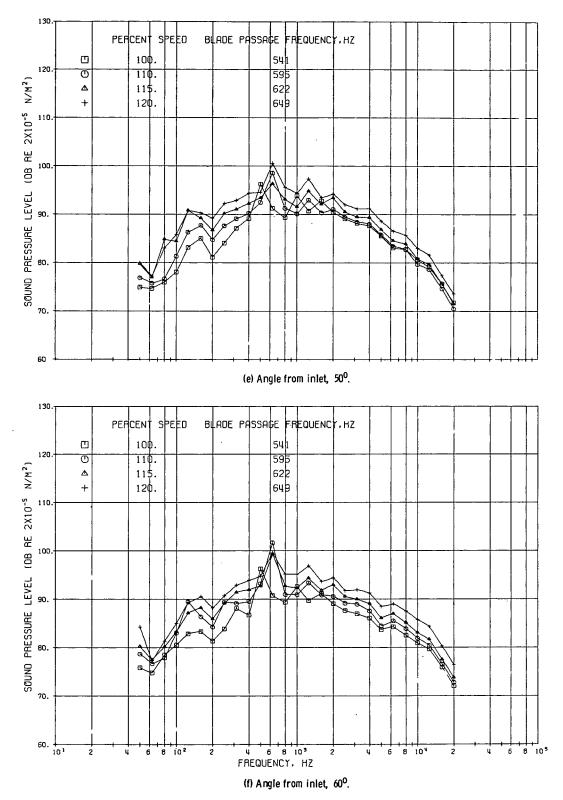


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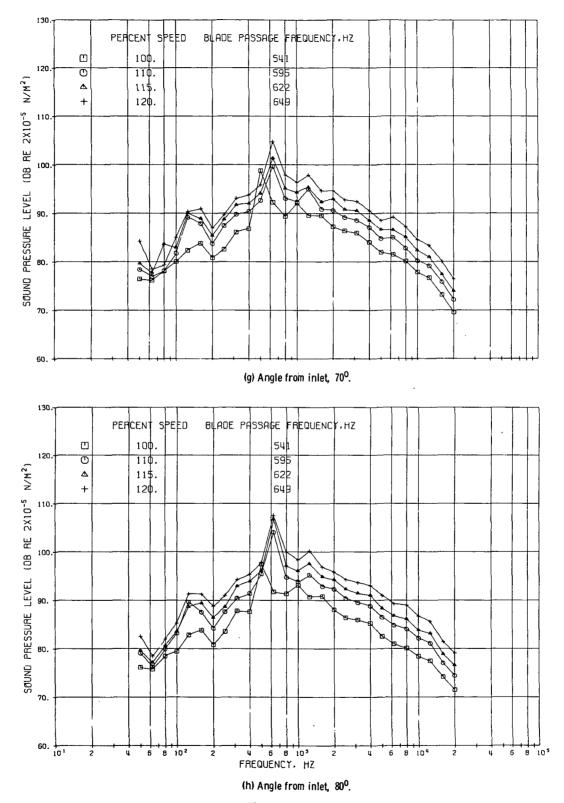


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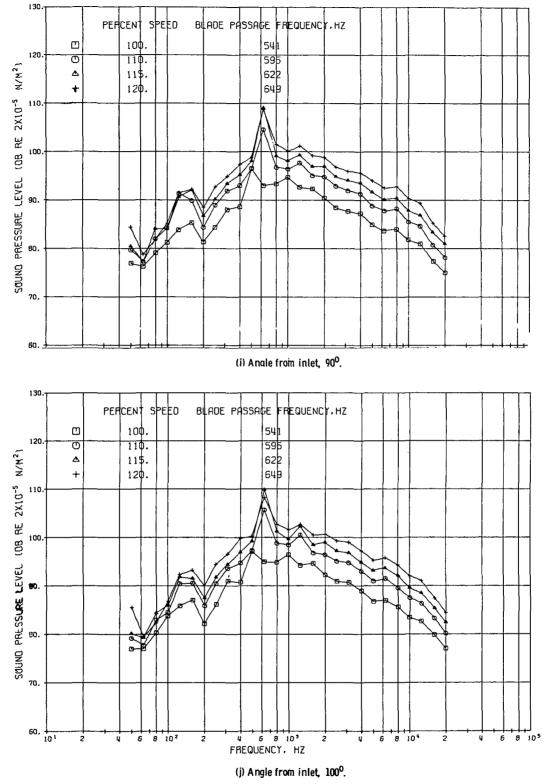


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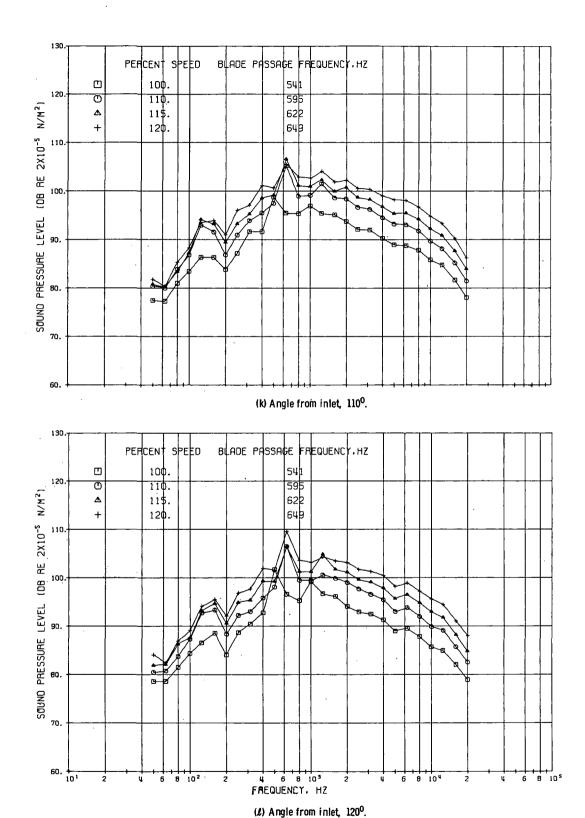


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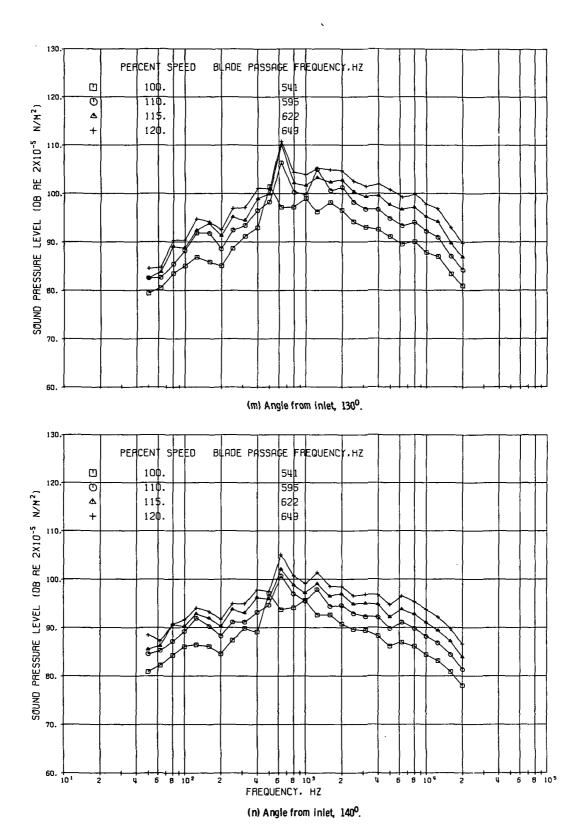


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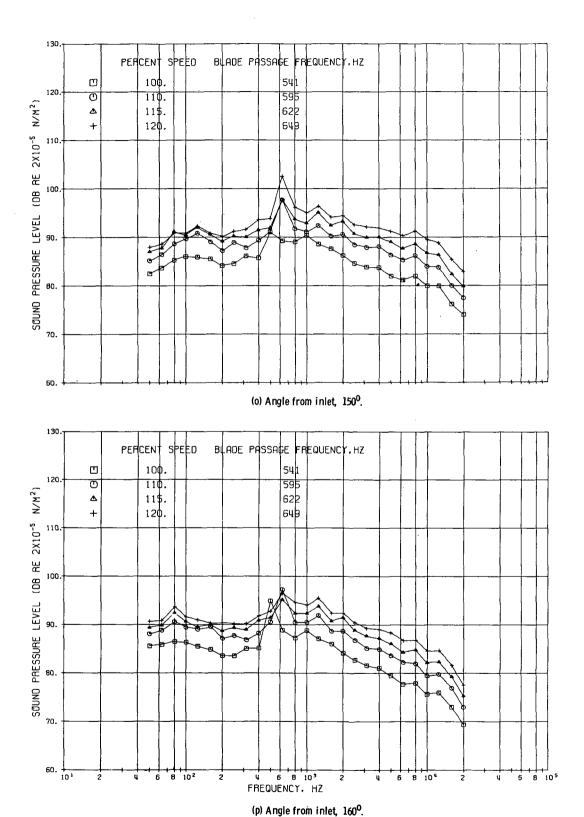


Figure 26. - Concluded.

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